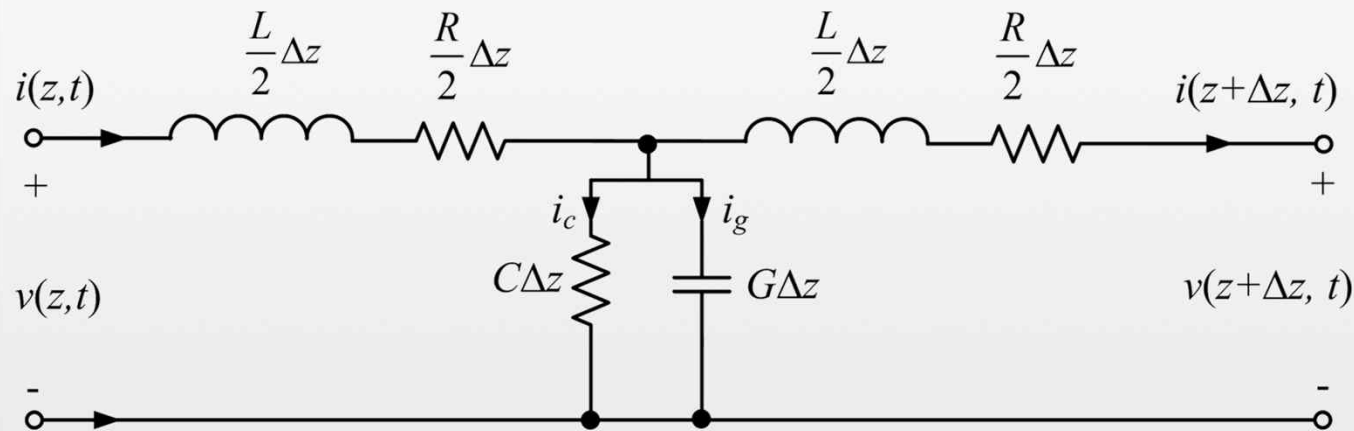


# Chapter 2

## Transmission Line

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## Learning Objectives

- Learn what the maximum power transmission condition is.
- Understanding real low loss transmission line
- Learn what is different for using lossy transmission instead of lossless transmission line

## Learning contents

- Maximum Power Transmission Condition
- Lossy Transmission Lines
- Terminated Lossy Transmission Line

# 1 Maximum Power Transmission Condition

- Lossless transmission line circuit with arbitrary generator and load impedances
  - Input impedance looking into terminated transmission line from generator:

$$Z_{in} = \frac{V_{in}}{I_{in}} = Z_0 \frac{Z_l + jZ_0 \tan \beta l}{Z_0 + jZ_l \tan \beta l}$$

- Let assume general source and load conditions:

$$Z_{in} = R_{in} + jX_{in} \text{ and } Z_g = R_g + jX_g$$

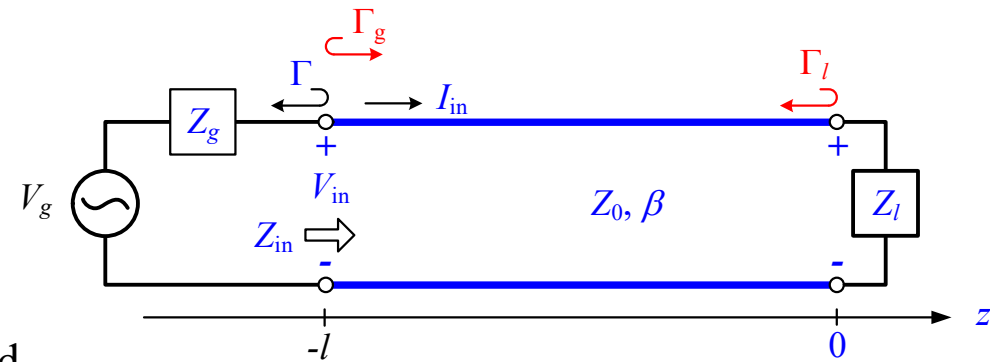
$$P = \frac{1}{2} |V_g|^2 \frac{R_{in}}{(R_{in} + R_g)^2 + (X_{in} + X_g)^2}$$

- Let's assume that the generator impedance ( $Z_g$ ) is only fixed.
- Power transmission for load matched to transmission line (case study 1)

$$P = \frac{1}{2} |V_g|^2 \frac{R_{in}}{(R_{in} + R_g)^2 + (X_{in} + X_g)^2} \Bigg|_{Z_l=Z_0=R_{in}} = \frac{1}{2} |V_g|^2 \frac{Z_0}{(Z_0 + R_g)^2 + X_g^2}$$

- Power transmission for generator matched to transmission line (case study 2)

$$P = \frac{1}{2} |V_g|^2 \frac{R_{in}}{(R_{in} + R_g)^2 + (X_{in} + X_g)^2} \Bigg|_{Z_g=Z_{in}} = \frac{1}{8} |V_g|^2 \frac{R_g}{R_g^2 + X_g^2}$$



# 1 Maximum Power Transmission Condition

- Power transmission for generator matched to transmission line (case study 3)

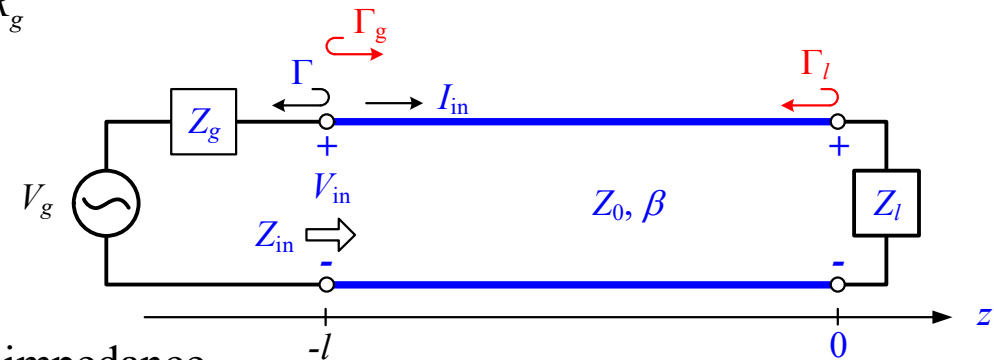
$$P = \frac{1}{2} |V_g|^2 \frac{R_{in}}{(R_{in} + R_g)^2 + (X_{in} + X_g)^2} \Big|_{R_{in}=R_g \text{ \& } X_{in}=-X_g} = \frac{1}{2} |V_g|^2 \frac{1}{4R_g}$$

- Maximum power condition: case study 3

$$Z_{in} = Z_g^*$$

→ **Conjugate matching**

→ **Maximum power transfer** to load for fixed generator impedance



cf.) 
$$P = \frac{1}{2} |V_g|^2 \frac{R_{in}}{(R_{in} + R_g)^2 + (X_{in} + X_g)^2} \Big|_{Z_l=Z_0=R_{in}} = \frac{1}{2} |V_g|^2 \frac{Z_0}{(Z_0 + R_g)^2 + X_g^2} \quad (\text{case study 1})$$

$$P = \frac{1}{2} |V_g|^2 \frac{R_{in}}{(R_{in} + R_g)^2 + (X_{in} + X_g)^2} \Big|_{Z_g=Z_{in}} = \frac{1}{2} |V_g|^2 \frac{R_g}{4(R_g^2 + X_g^2)} \quad (\text{case study 2})$$

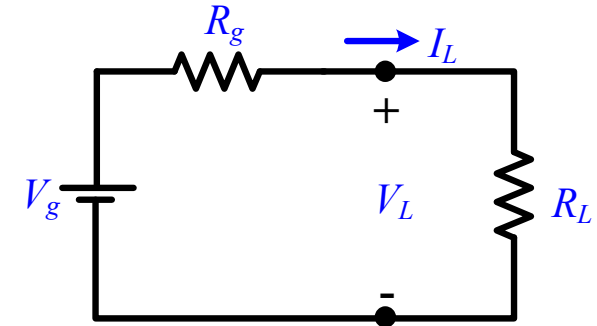
# 1 Maximum Power Transmission Condition

- Maximum power transfer condition for DC related circuit in condition of fixed source resistance

$$V_L = V_g \frac{R_L}{R_g + R_L}, \quad I_L = \frac{V_g}{R_g + R_L}$$

$$P_L = I_L V_L = V_g^2 \frac{R_L}{(R_g + R_L)^2}$$

$$P_{L, \max} = \frac{dP_L}{dR_L} = V_g^2 \frac{(R_g + R_L)^2 - 2R_L(R_g + R_L)}{(R_g + R_L)^4} = V_g^2 \frac{R_g^2 - R_L^2}{(R_g + R_L)^4} = 0 \Leftrightarrow R_g = R_L$$



→ The condition for the maximum DC power transferring to load is for *same source and load resistances*.

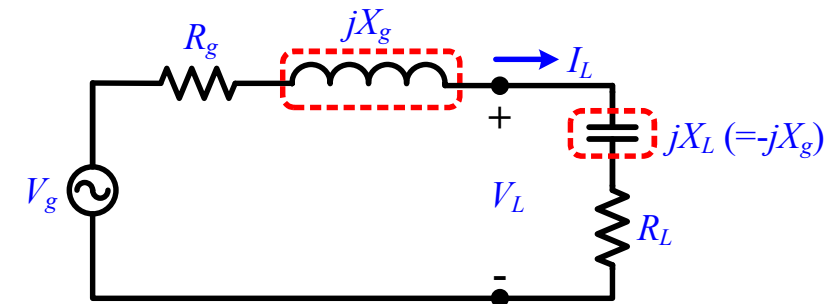
- Maximum power transfer condition for AC or microwave circuit

$$Z_L = Z_g^* \quad \text{or} \quad Z_g = Z_L^*$$

$$\Leftrightarrow Z_L = R_L + jX_L = R_g - jX_g^*$$

→ The maximum microwave power transfer condition is same with the maximum DC power transfer condition **except resonance condition**.

→ *Frequency selective maximum power delivery condition*



## 2 Lossy Transmission Lines

- Effects of loss on transmission line behavior
- How many the attenuation constant can be calculated?

- General complex propagation constant:

$$\begin{aligned}\gamma &= \alpha + j\beta = \sqrt{(R + j\omega L)(G + j\omega C)} \\ &= \sqrt{(j\omega L)(j\omega C)\left(1 + \frac{R}{j\omega L}\right)\left(1 + \frac{G}{j\omega C}\right)} = j\omega\sqrt{LC} \sqrt{1 - j\left(\frac{R}{\omega L} + \frac{G}{\omega C}\right) - \frac{RG}{\omega^2 LC}}\end{aligned}$$

$$\beta = j\omega\sqrt{LC} \sqrt{1 - \frac{RG}{\omega^2 LC}}$$

- $\beta$  is not a linear function of frequency (e.g.,  $\beta \neq a\omega$ ).
  - ➔ Phase velocity ( $v_p = \omega / \beta$ ) will be different for different frequencies  $\omega$ .
  - ➔ The various frequency components of a wideband signal will travel with different phase velocities.
  - ➔ The arrival at the receiver end of the transmission line is at slightly different times. ➔ **Dispersion** (: a distortion of the signal)
  - ➔ Undesirable effect

## 2 Lossy Transmission Lines

- For low-loss transmission line ( $R \ll \omega L$ ,  $G \ll \omega C$ ) ( $\Leftrightarrow$  low conductor loss and low dielectric loss),

$$\gamma \cong j\omega\sqrt{LC} \sqrt{1 - j\left(\frac{R}{\omega L} + \frac{G}{\omega C}\right)} \quad \leftarrow RG \ll \omega^2 LC$$

By using  $\sqrt{1+x} \approx 1 + x/2 + \dots$ ,

$$\gamma = \alpha + j\beta \approx j\omega\sqrt{LC} \left[ 1 - \frac{j}{2} \left( \frac{R}{\omega L} + \frac{G}{\omega C} \right) \right]$$

$$\alpha \approx \frac{1}{2} \left( R\sqrt{\frac{C}{L}} + G\sqrt{\frac{L}{C}} \right) = \frac{1}{2} \left( \frac{R}{Z_0} + GZ_0 \right), \quad \beta = \omega\sqrt{LC}$$

$\rightarrow$   $\beta$  of low loss transmission line is almost similar to lossless transmission line.

where  $Z_0 = (L/C)^{0.5}$ : characteristic impedance of lossless transmission line

$\alpha$ : attenuation constant

$\beta$ : phase constant

### 3 Terminated Lossy Transmission Line

- Lossy transmission line terminated in a load impedance  $Z_L$ 
  - Complex propagation constant :  $\gamma = \alpha + j\beta$
  - Assumption: low loss transmission line ( $Z_0 \approx \sqrt{\frac{L}{C}}$ )
  - Voltage and current waves on low loss transmission line

$$V(z) = V_0^+ [e^{-\gamma z} + \Gamma e^{\gamma z}]$$

$$I(z) = \frac{V_0^+}{Z_0} [e^{-\gamma z} - \Gamma e^{\gamma z}]$$

where  $\Gamma$ : reflection coefficient at load ( $= (Z_L - Z_0) / (Z_L + Z_0)$ ),

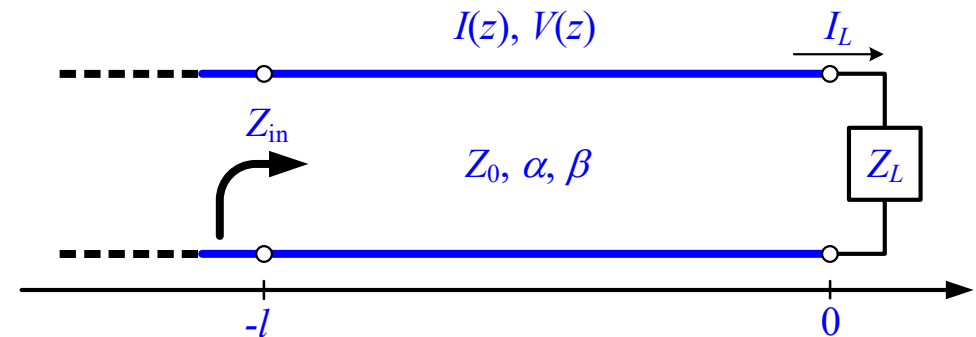
$V_0^+$ : incident voltage amplitude referenced at  $z = -l$

- Reflection coefficient at a distance  $l$  from load:

$$\Gamma(-l) = \Gamma e^{-2j\beta l} e^{-2\alpha l} = \Gamma e^{-2\gamma l}$$

- Input impedance  $Z_{in}$  at a distance  $l$  from load:

$$Z_{in} = \frac{V(-l)}{I(-l)} = Z_0 \frac{Z_L + Z_0 \tanh \gamma l}{Z_0 + Z_L \tanh \gamma l}$$





### 3 Terminated Lossy Transmission Line

- Power delivered to input of terminated line at  $z = -l$ :

$$P_{\text{in}} = \frac{1}{2} \text{Re} [V(-l)I^*(-l)] = \frac{|V_0^+|^2}{2Z_0} \text{Re} [(e^{\gamma l} + \Gamma e^{-\gamma l})(e^{\gamma^* l} - \Gamma^* e^{-\gamma^* l})] \leftarrow \gamma = \alpha + j\beta$$

$$= \frac{|V_0^+|^2}{2Z_0} \text{Re} [(e^{\alpha l} e^{j\beta l} + \Gamma e^{-\alpha l} e^{-j\beta l})(e^{\alpha l} e^{-j\beta l} - \Gamma^* e^{-\alpha l} e^{j\beta l})]$$

$$= \frac{|V_0^+|^2}{2Z_0} \text{Re} \{ (e^{2\alpha l} - |\Gamma|^2 e^{-2\alpha l} + \Gamma e^{-2j\beta l} - \Gamma^* e^{j2\beta l}) \}$$

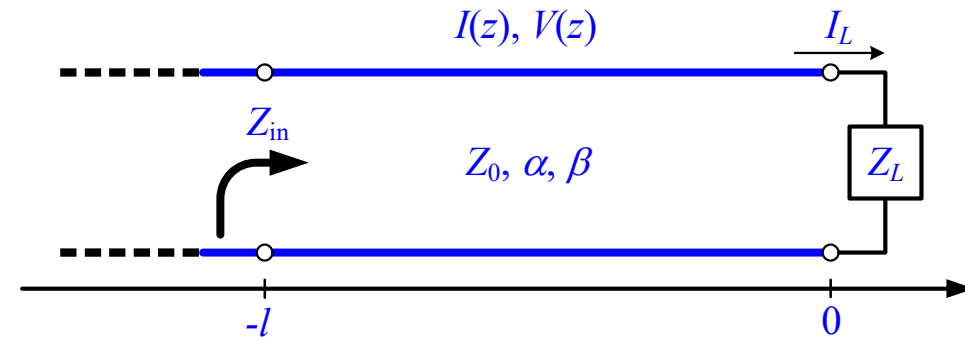
$$= \frac{|V_0^+|^2}{2Z_0} [e^{2\alpha l} - |\Gamma|^2 e^{-2\alpha l}] \leftarrow |\Gamma|^2 = \Gamma(0) \cdot \Gamma^*(0) = |\Gamma(-l)|^2 e^{4\alpha l}, \Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}$$

$$= \frac{|V_0^+|^2}{2Z_0} [1 - |\Gamma(-l)|^2] e^{2\alpha l}$$

- Power delivered to load:  $P_L = \frac{1}{2} \text{Re} [V(0)I^*(0)] = \frac{|V_0^+|^2}{2Z_0} (1 - |\Gamma|^2)$

- Power loss through transmission line:  $P_{\text{loss}} = P_{\text{in}} - P_L = \frac{|V_0^+|^2}{2Z_0} [(e^{2\alpha l} - 1) + |\Gamma|^2 (1 - e^{-2\alpha l})]$

- If  $\alpha \uparrow$ , also  $P_{\text{loss}} \uparrow$



Incident wave  
power loss

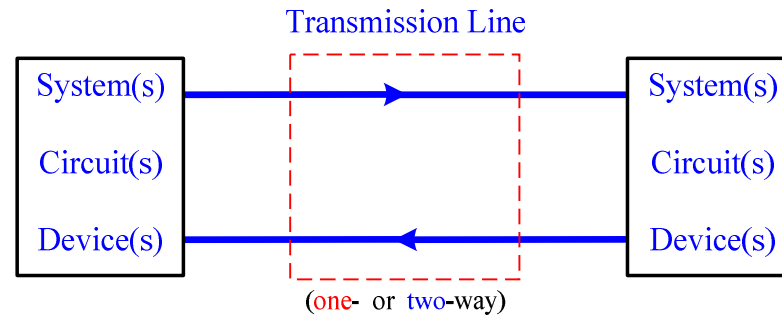
Reflected wave  
power loss

## 4 Review

- Impedance matching
  - $Z_{in} = Z_g^*$  or  $Z_g = Z_{in}^*$ 
    - $\Leftrightarrow Z_{in} = R_{in} + jX_{in} = R_g - jX_g^*$
  - At any reference plane
- Low loss transmission line
  - It is important to understand why smallest transmission line is used.
  - Signal loss and distortion
  - Incident and reflected wave power loss

## 5 Chapter Review

- **Transmission line (TRL):** carrier to transmit electric energy, signals, data, and information from one point to another point with small insertion loss



- Analyzing approaches

- 1) Maxwell's equations: electromagnetic field method (complete & accurate)
- 2) Circuit equations: equivalent voltage and current analysis method (intuitive & inaccurate)

- General lumped elements ( $R$ ,  $L$ ,  $C$ , etc.) frequency dependent characteristics  $\rightarrow$  SRF

- Characteristic impedance: a ratio of voltage wave to current wave  $Z_0 = \frac{V_o^+}{I_o^+} = -\frac{V_o^-}{I_o^-} = \frac{R + j\omega L}{\gamma} = \sqrt{\frac{R + j\omega L}{G + j\omega C}} \neq R_0$

- Complex propagation constant:  $\gamma = \alpha + j\beta = \sqrt{(R + j\omega L)(G + j\omega C)} = f(\omega)$

# 5 Chapter Review

- Voltage reflection coefficient ( $\Gamma$ ) = Reflected voltage wave amplitude / Incident voltage wave amplitude

$$\Gamma = \frac{V_0^-}{V_0^+} = \frac{|V_0^-| e^{j\phi^-}}{|V_0^+| e^{j\phi^+}} = \frac{Z_L - Z_0}{Z_L + Z_0} = |\Gamma| e^{j\theta}$$

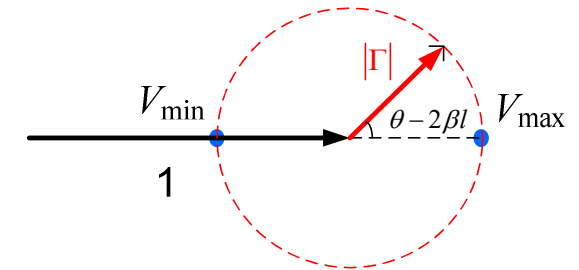
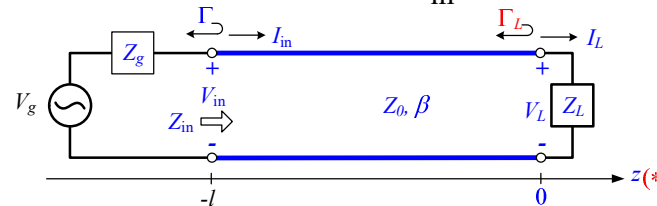
- **If  $\Gamma = 0$ , no reflected wave.  $\rightarrow Z_L = Z_0$  ((Impedance) Matching!!)**

- (Voltage) Standing wave ratio (VSWR):  $SWR = \frac{V_{\max}}{V_{\min}} = \frac{1+|\Gamma|}{1-|\Gamma|}$

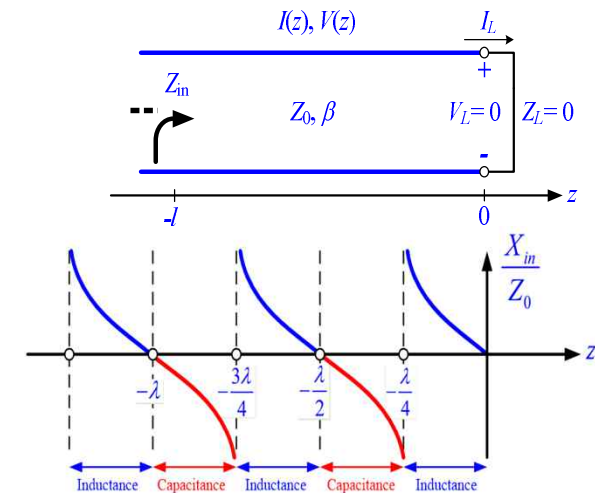
- Two successive voltage maxima (or minima) on TRL:  $l = \lambda / 2$

- Input impedance seen looking toward the load at  $z = -l$ :  $Z_{in}$

$$Z_{in} = Z_0 \frac{Z_L + jZ_0 \tan \beta l}{Z_0 + jZ_L \tan \beta l}$$



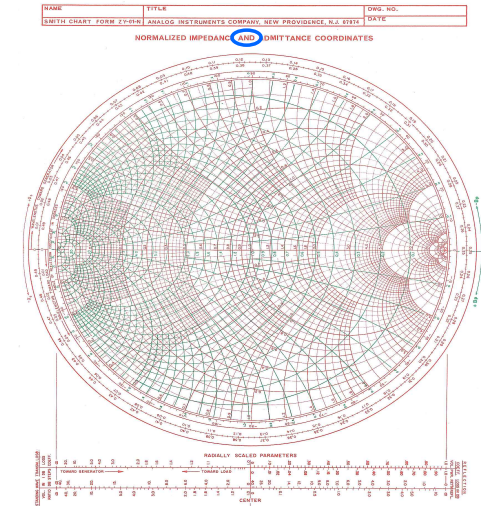
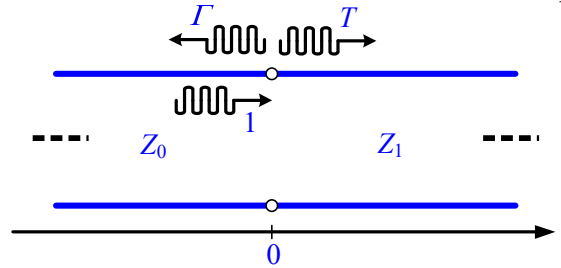
- TRL terminated with short or open circuit can be used inductor or capacitor in microwave frequency range.
  - Frequency and transmission line length dependent
  - Periodic characteristics



# 5 Chapter Review

- TRL of characteristic impedance  $Z_0$  connected different characteristic impedance ( $Z_1$ ) transmission line

- Reflection coefficient:  $\Gamma = \frac{Z_1 - Z_0}{Z_1 + Z_0}$
- Reflection and transmission



- Smith chart
  - Reflection coefficient plane
  - Analyzing approaches for visualizing transmission line phenomenon
  - Intuition about transmission line and impedance-matching problems

- Slotted TRL
  - Waveguide, coaxial cable
  - Measurement issues: (V)SWR, distance of (first) voltage maximum (or minimum) from load,  $Z_L$ ,  $\lambda$ , etc.
  - In real condition, network analyzer is used generally.

- Maximum power transmission condition: impedance conjugate matching

$$Z_{in} = Z_g^*$$

- Lossy TRL:  $P_{loss} = P_{in} - P_L = \frac{|V_0^+|^2}{2Z_0} \left[ (e^{2\alpha l} - 1) + |\Gamma|^2 (1 - e^{-2\alpha l}) \right]$

