

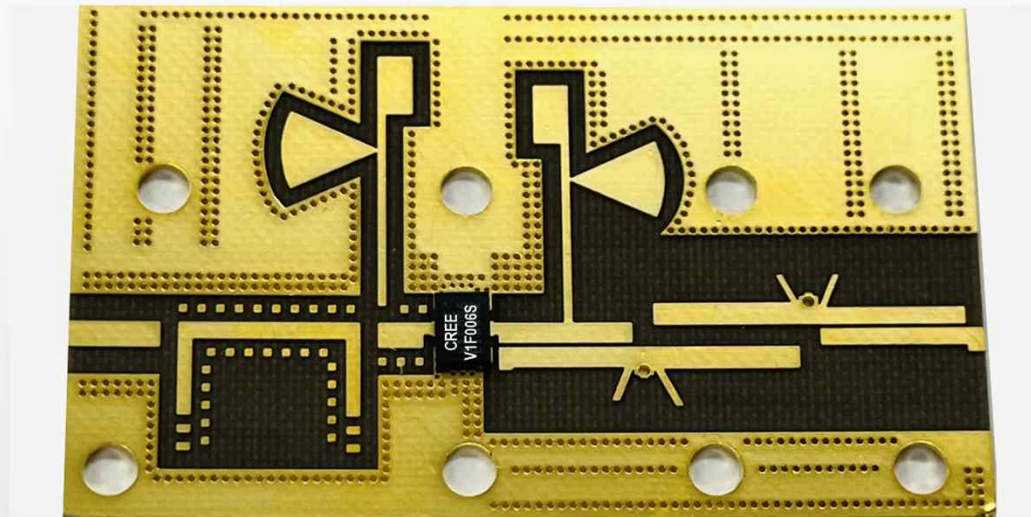
# Chapter 5

# Impedance Matching

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## Learning Objectives

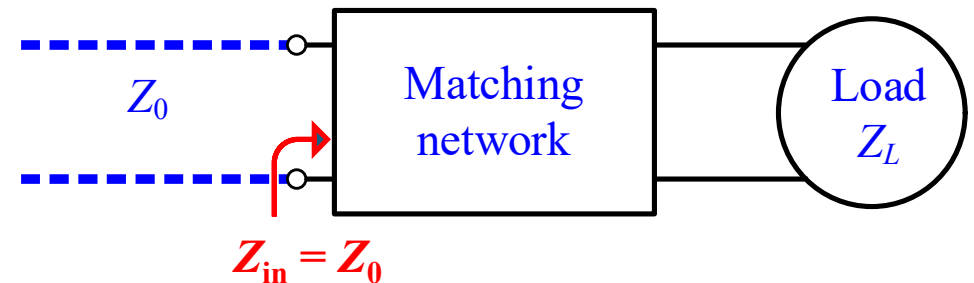
- Learn why impedance matching is important in system viewpoints.
- Learn how impedance matching can be done.
- Understanding real microwave lumped elements

## Learning contents

- Matching Network with Lumped Elements (L-section)
- Impedance Matching Example using Calculation and Smith Chart
- Microwave Lumped Elements

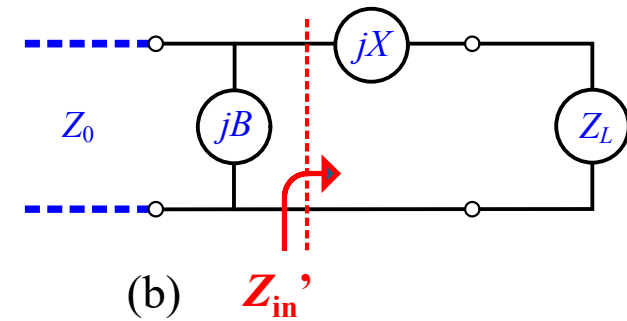
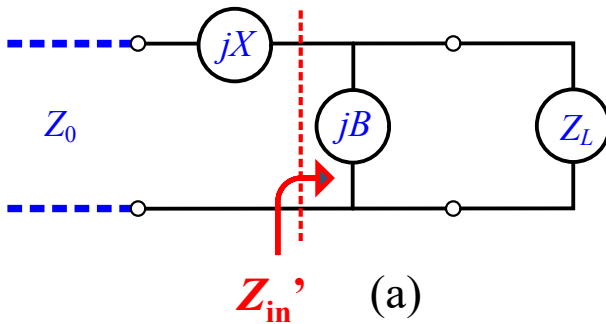
# 1 Usefulness of Impedance Matchings

- Matching network usefulness
  - The **maximum power** is delivered when the load is matched to the transmission line (assuming the generator is matched), and power loss in the feed line is minimized.
  - Impedance matching sensitive receiver components (antenna, low-noise amplifier, etc.) **improves the signal-to-noise ratio(SNR)** of the receiving system.
  - Impedance matching in a power distribution network (such as an antenna array feed network) will **reduce amplitude and phase errors spatially**.
- Important factors in selection of particular matching network
  - Complexity: simple
  - Bandwidth: restricted/broad/multi frequency band
  - Implementation: easy
  - Adjustability: tunable



## 2 Matching Network with Lumped Elements (*L*-section)

- L-section matching network
  - Simplest matching network including two reactive elements
  - Normalized load impedance:  $z_L = Z_L / Z_0$  and  $Z_L = R_L + jX_L$
  - $X$  and  $B$ : lumped or distributed (reactive and susceptive) element depending on operating frequency
  - Matching network for (a)  $z_L$  inside of  $1 + jx$  circle and (b)  $z_L$  outside of  $1 + jx$  circle on Smith chart



- For (a),

$$Z_{in}' = Z_L // \frac{1}{jB} = \frac{Z_L / jB}{Z_L + \frac{1}{jB}} = \frac{Z_L}{1 + jBZ_L}$$

$$\text{Re}[Z_{in}'] < R_L$$

For (b),

$$Z_{in}' = (Z_L + jX) // \frac{1}{jB} = \frac{(Z_L + jX) / jB}{(Z_L + jX) + \frac{1}{jB}} = \frac{Z_L + jX}{1 + jB(Z_L + jX)}$$

$$\text{Re}[Z_{in}'] > R_L$$

## 2 Matching Network with Lumped Elements (L-section)

- Smith chart: reflection coefficient plane

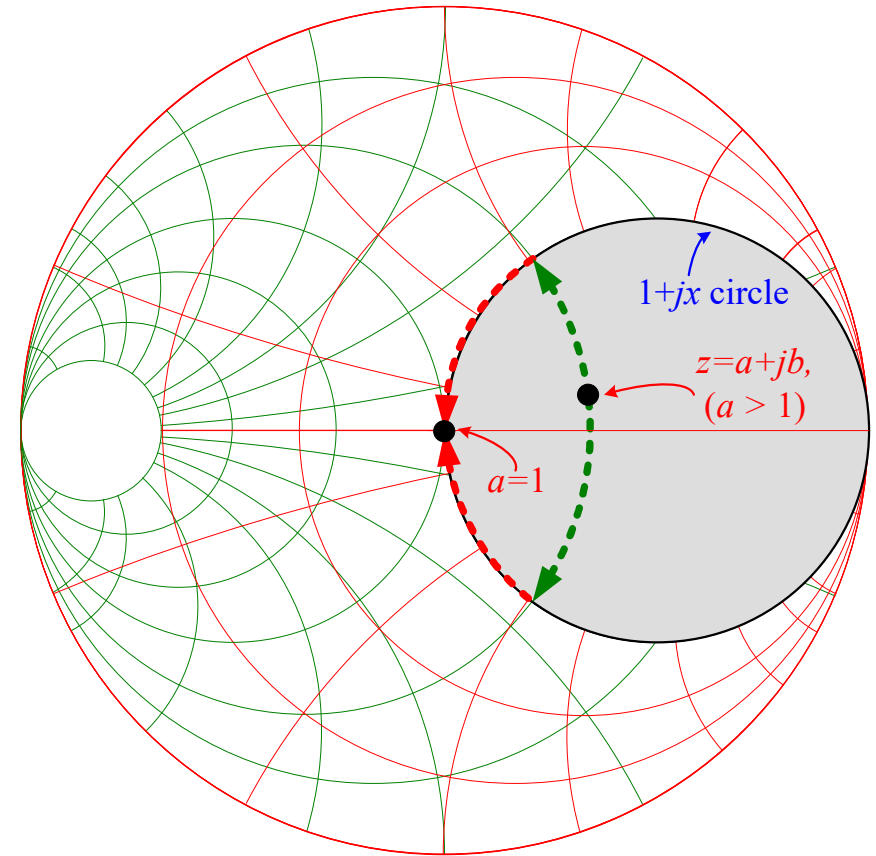
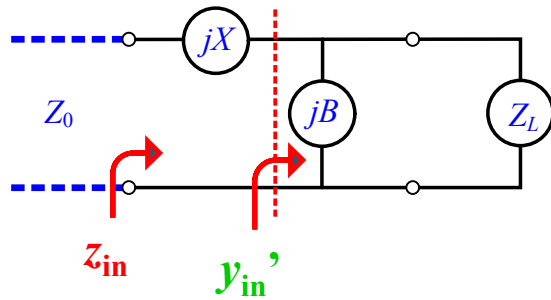
$$\Gamma = \Gamma_r + j\Gamma_i Z_L \stackrel{\text{or}}{=} |\Gamma| e^{j\phi}$$

$$z = r + jx$$

- Matching condition:  $|\Gamma| = 0$  or  $z = 1 + j0$  ( $\Leftrightarrow y = 1 + j0$ )

- For  $z_L$  inside of  $1 + jx$  circle ( $r_L > 1$ ),

$$z_L \rightarrow y_{in}' = 1 + jx \text{ circle} \rightarrow z_{in} = 1 + j0$$



## 2 Matching Network with Lumped Elements ( $L$ -section)

- Smith chart: reflection coefficient plane

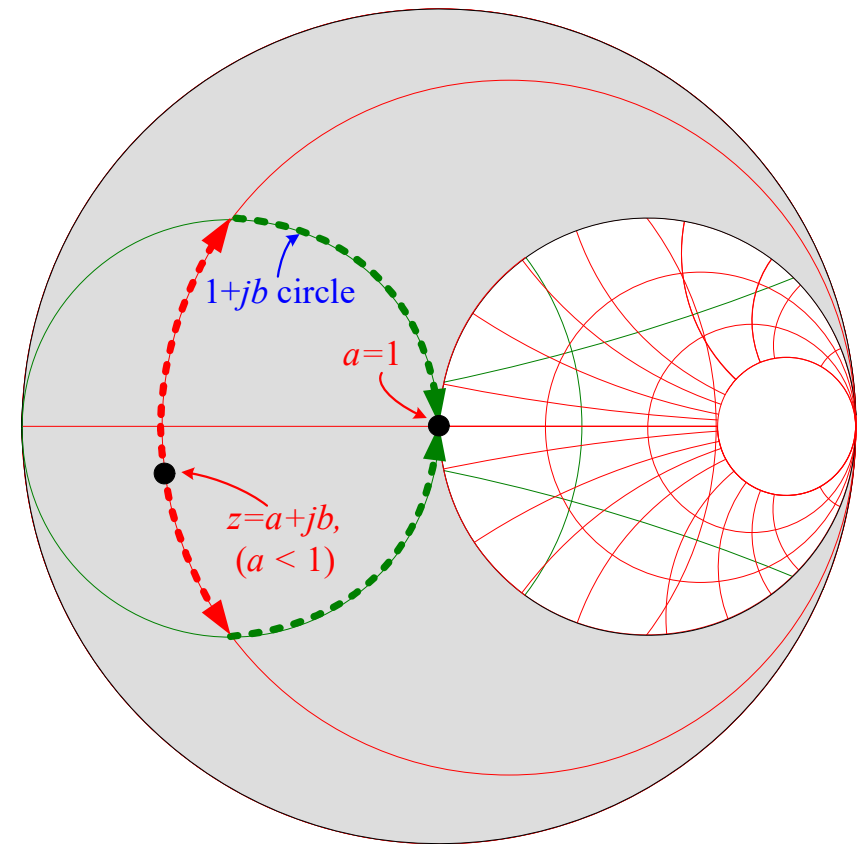
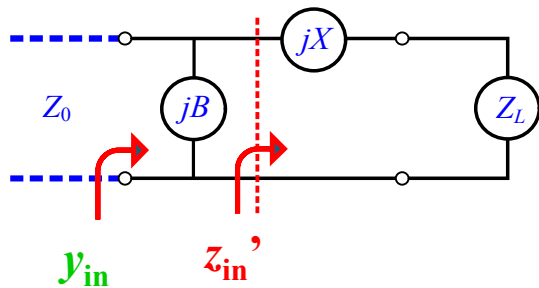
$$\Gamma = \Gamma_r + j\Gamma_i Z_L \stackrel{\text{or}}{=} |\Gamma| e^{j\phi}$$

$$z = r + jx$$

- Matching condition:  $|\Gamma| = 0$  or  $z = 1 + j0$  ( $\Leftrightarrow y = 1 + j0$ )

- For  $z_L$  outside of  $1 + jx$  circle ( $r_L < 1$ ),

$$z_L \rightarrow z_{in}' = 1 + jb \text{ circle} \rightarrow y_{in} = 1 + j0$$



## 2 Matching Network with Lumped Elements (L-section)

- Analytic solution for  $z_L$  inside  $1 + jx$  circle ( $r_L > 1$ )

-  $Z_L = R_L + jX_L$  (assumption:  $Z_0 < R_L$ )

- Input impedance seen looking into the matching network:

$$Z_{in} = Z_0$$

$$= jX + \frac{1}{jB + 1/(R_L + jX_L)}$$

$$Z_0 - jX = \frac{R_L + jX_L}{(1 - BX_L) + jBR_L}$$

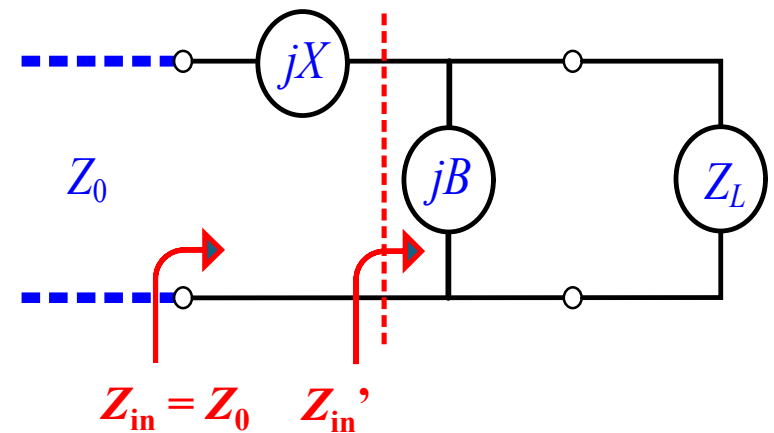
$$(Z_0 - jX)\{(1 - BX_L) + jBR_L\} = R_L + jX_L$$

$$\{Z_0 + B(R_L X - X_L Z_0)\} + j\{BR_L Z_0 - X(1 - BX_L)\} = R_L + jX_L$$

- Rearranging and separating into real and imaginary parts:

$$\text{real part: } B(R_L X - X_L Z_0) = R_L - Z_0$$

$$\text{imaginary part: } X(1 - BX_L) = BR_L Z_0 - X_L$$



## 2 Matching Network with Lumped Elements ( $L$ -section)

- Solving and substituting  $X$  for  $B$

$$B = \frac{X_L (\pm) \sqrt{R_L / Z_0} \sqrt{R_L^2 + X_L^2 - Z_0 R_L}}{R_L^2 + X_L^2}$$

where  $R_L^2 + X_L^2 - Z_0 R_L > 0$  ( $\because R_L > Z_0$ )

$$X = \frac{BX_L Z_0 + R_L - Z_0}{BR_L} = \frac{1}{B} + \frac{X_L Z_0}{R_L} - \frac{Z_0}{BR_L}$$

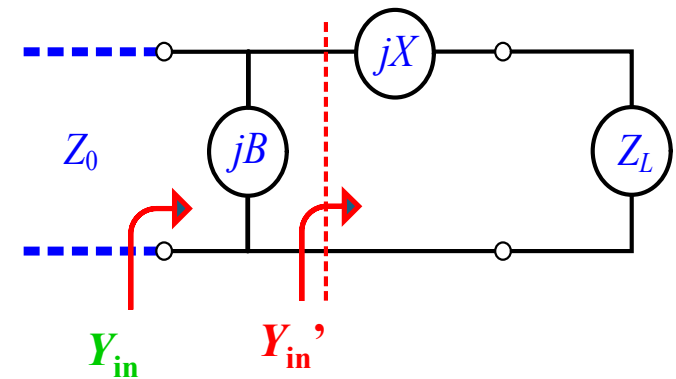
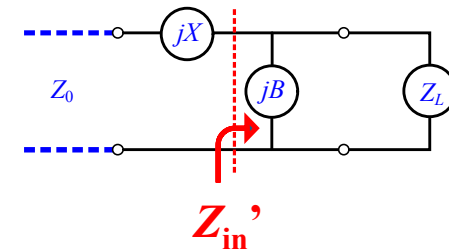
→ Two solutions: dual valued components ( $B, X$ )

▪ Analytic solution for  $z_L$  outside  $1 + jx$  circle ( $r_L < 1$ )

- Input admittance seen looking into the matching network:

$$Y_{in} = jB + \frac{1}{R_L + j(X + X_L)} \quad \leftarrow Z_L = R_L + jX_L$$

$$= \frac{1}{Z_0}$$





## 2 Matching Network with Lumped Elements (L-section)

- Rearranging and separating into real and imaginary parts:

$$BZ_0(X + X_L) = Z_0 - R_L$$

$$(X + X_L) = BZ_0R_L$$

- Solving for  $X$  and  $B$ :

$$X = \pm \sqrt{R_L(Z_0 - R_L)} - X_L$$

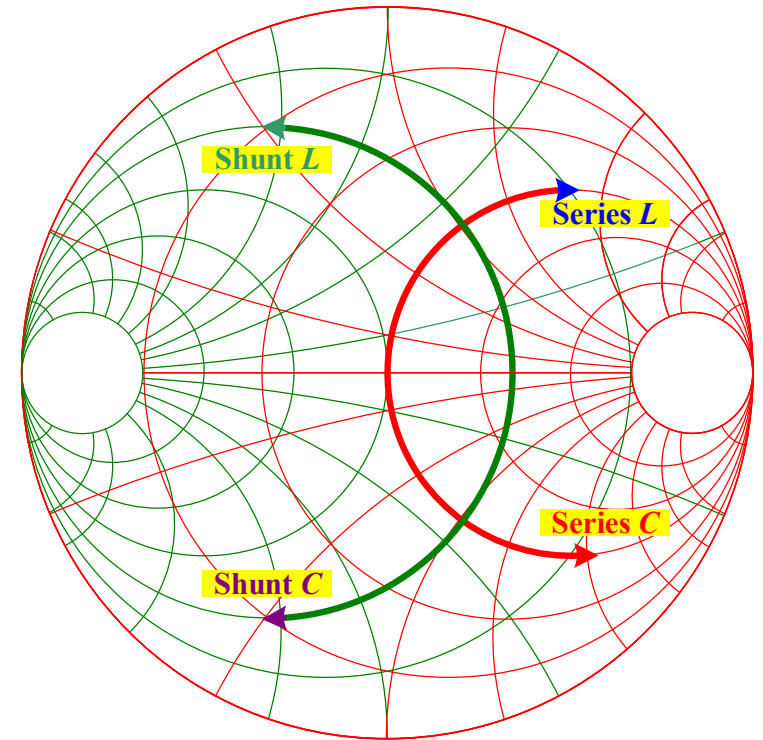
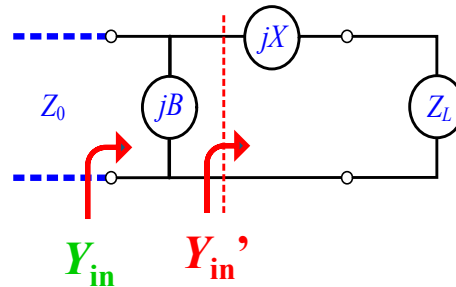
$$B = \pm \sqrt{(Z_0 - R_L) / R_L} / Z_0$$

→ Two solutions: dual valued components ( $B, X$ )

- Addition series L/C on fixed impedance and shunt L/C on fixed admittance

$$Z + j\omega L \text{ (or } -j\frac{1}{\omega C} \text{)} = R + j(X + \omega L) \text{ (or } R + j(X - \frac{1}{\omega C} \text{))}$$

$$Y + j\omega C \text{ (or } -j\frac{1}{\omega L} \text{)} = G + j(B + \omega C) \text{ (or } G + j(B - \frac{1}{\omega L} \text{))}$$



## 3

## Impedance Matching Example using Calculation and Smith Chart

- Design an  $L$ -section matching network to match a series  $RC$  load with an impedance  $Z_L = 100 + j200$  [ $\Omega$ ] to 50 [ $\Omega$ ] transmission line at a frequency of 1 GHz.

### 1) Theoretical solutions

- Characteristic admittance:  $Y_0 = \frac{1}{Z_0} = \frac{1}{50} = 0.02$

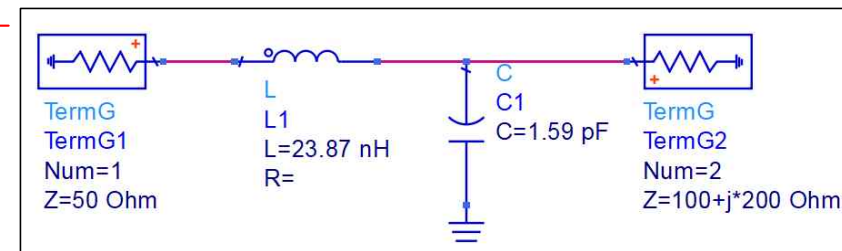
⇒ **Solution #01:** (series  $L$  & shunt  $C$ ) can be found

$$- B = \frac{X_L + \sqrt{R_L / Z_0} \sqrt{R_L^2 + X_L^2 - Z_0 R_L}}{R_L^2 + X_L^2} = \frac{200 + \sqrt{100 / 50} \times \sqrt{100^2 + 200^2 - 50 \times 100}}{100^2 + 200^2} = 0.01 \rightarrow b = \frac{B}{Y_0} = \frac{0.01}{0.02} = 0.5$$

$$- X = \frac{1}{B} + \frac{X_L Z_0}{R_L} - \frac{Z_0}{B R_L} = \frac{1}{0.01} + \frac{200 \times 50}{100} - \frac{50}{0.01 \times 100} = 150 \rightarrow x = \frac{X}{Z_0} = \frac{150}{50} = 3$$

$$\rightarrow C = \frac{b}{2\pi f Z_0} = \frac{0.5}{2\pi \times 10^9 \times 50} = 1.59 \text{ pF} \leftarrow B = b Y_0 = \frac{b}{Z_0} = \omega C, C = \frac{b}{\omega Z_0}$$

$$\rightarrow L = \frac{x Z_0}{2\pi f} = \frac{3 \times 50}{2\pi \times 10^9} = 23.87 \text{ nH} \leftarrow X = x Z_0 = \omega L, L = \frac{x Z_0}{\omega}$$



## 3

## Impedance Matching Example using Calculation and Smith Chart

## 1) Theoretical solutions

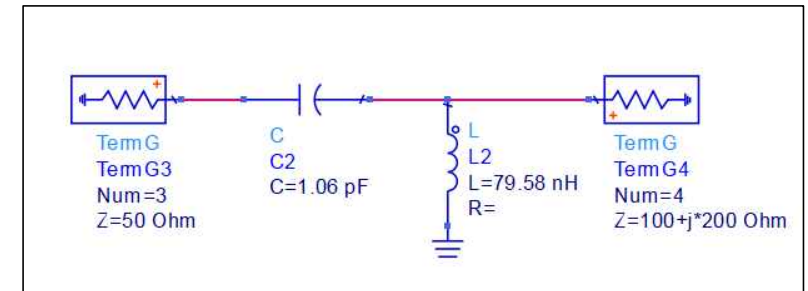
⇒ **Solution #02:** (series  $C$  & shunt  $L$ ) can be found

$$- B = \frac{X_L \left( -\sqrt{R_L / Z_0} \sqrt{R_L^2 + X_L^2 - Z_0 R_L} \right)}{R_L^2 + X_L^2} = \frac{200 + \sqrt{100 / 50} \times \sqrt{100^2 + 200^2 - 50 \times 100}}{100^2 + 200^2} = -0.002 \rightarrow b = \frac{B}{Y_0} = \frac{-0.002}{0.02} = -0.1$$

$$- X = \frac{1}{B} + \frac{X_L Z_0}{R_L} - \frac{Z_0}{B R_L} = \frac{1}{-0.002} + \frac{200 \times 50}{100} - \frac{50}{-0.002 \times 100} = -150 \rightarrow x = \frac{X}{Z_0} = \frac{150}{50} = -3$$

$$\rightarrow C = -\frac{1}{2\pi f x Z_0} = -\frac{1}{2\pi \times 10^9 \times (-3) \times 50} = 1.06 \text{ pF} \quad \leftarrow jX = jxZ_0 = -j \frac{1}{\omega C}, \quad C = -\frac{1}{\omega x Z_0}$$

$$\rightarrow L = -\frac{Z_0}{2\pi f b} = -\frac{50}{2\pi \times 10^9 \times (-0.1)} = 79.58 \text{ nH} \quad \leftarrow jB = jbY_0 = \frac{jb}{Z_0} = -j \frac{1}{\omega L}, \quad L = -\frac{Z_0}{\omega b}$$



### 3 Impedance Matching Example using Calculation and Smith Chart

#### 2) Smith chart solutions

$$- Z_L = 100 + j200 \rightarrow z_L = \frac{Z_L}{Z_0} = 2 + j4 \rightarrow y_L = \frac{1}{z_L} = 0.1 - j0.2$$

⇒ **Solution #01:** (Denoted by blue color on Smith chart)

$$- y = y_L + jb = \frac{1}{z} = (0.1 - j0.2) + j0.5 = 0.1 + j0.3 \leftarrow b = 0.5$$

- Interconnection with impedance circle of  $1 - jx$

$$z_{in} = z + jx = (1 - j3) + j3 = 1 - j0 \rightarrow x = 3$$

⇒ **Solution #02:** (Denoted by pink color on Smith chart)

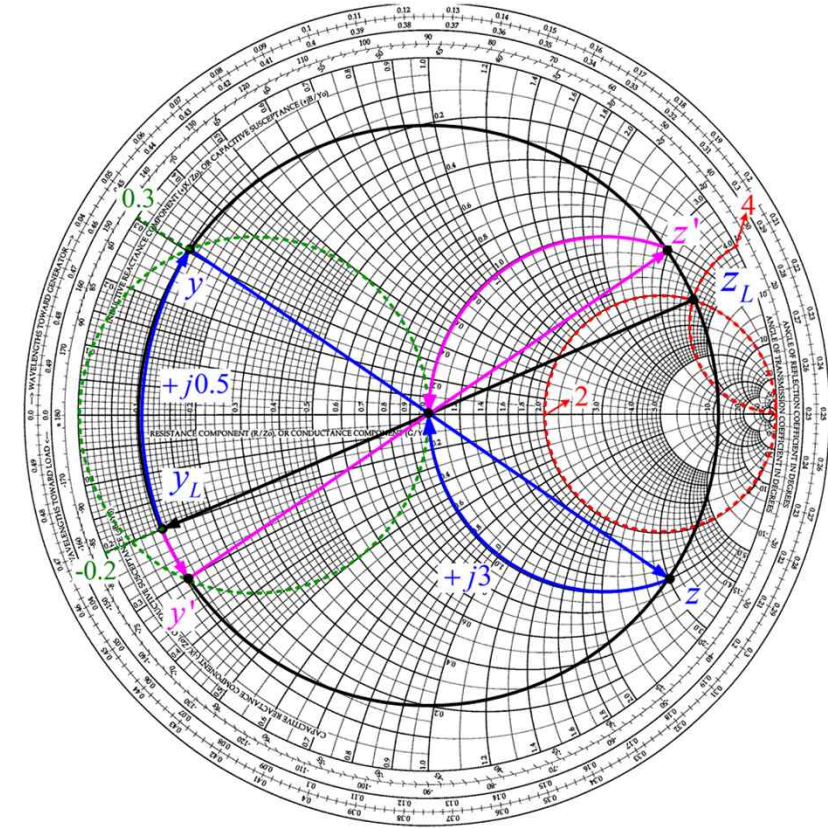
$$- y' = y_L + jb' = \frac{1}{z'} = (0.1 - j0.2) - j0.1 = 0.1 - j0.3 \leftarrow jb' = -j0.1$$

- Interconnection with impedance circle of  $1 + jx$

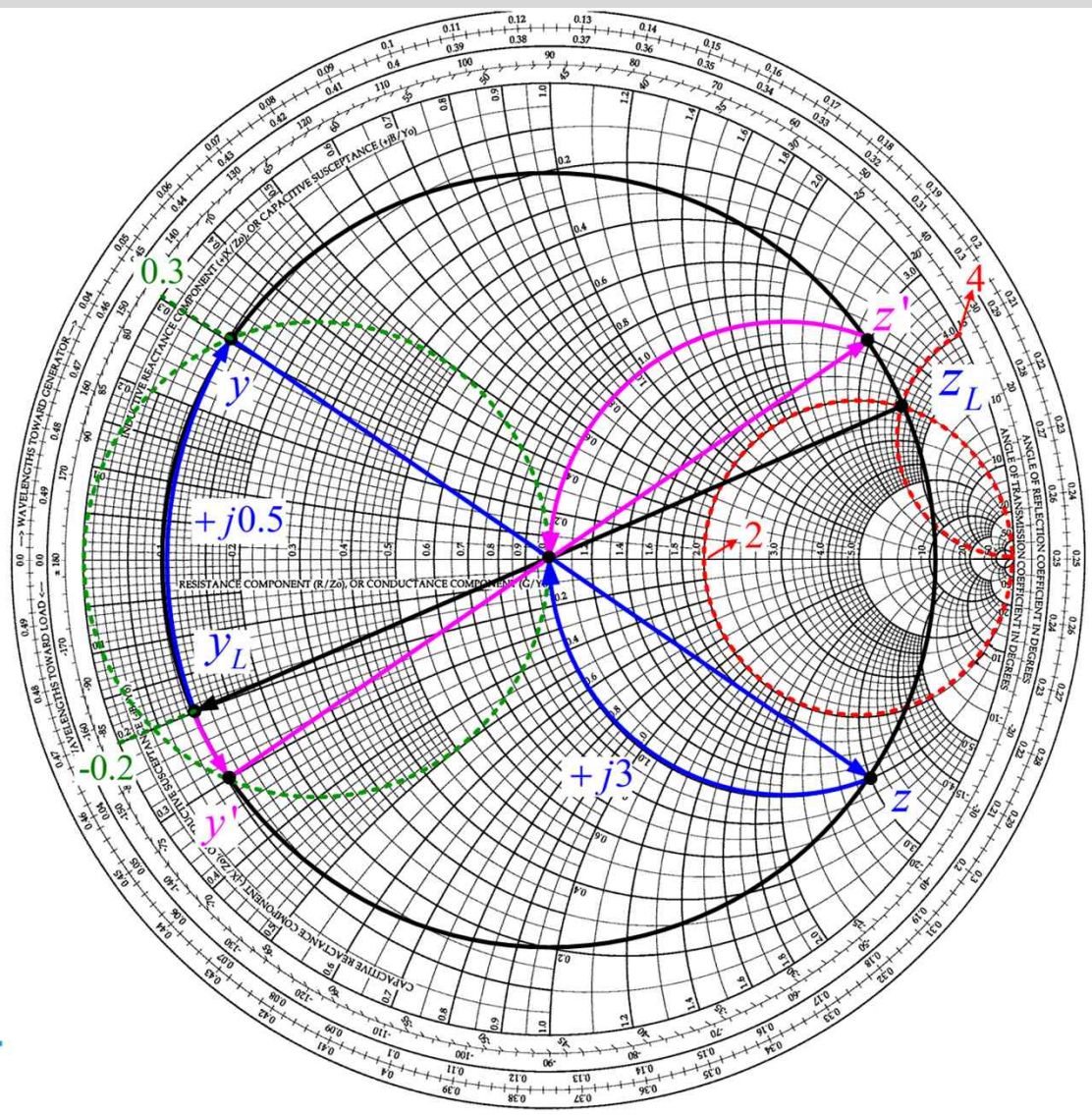
$$z_{in} = z' + jx = (1 + j3) - j3 = 1 + j0 \rightarrow x = -3$$

⇒ Finally,  $L$  &  $C$  can be found by using these formula:

$$C = \frac{b}{2\pi f Z_0}, L = \frac{x Z_0}{2\pi f} : \text{approximately same with theoretical solution}$$



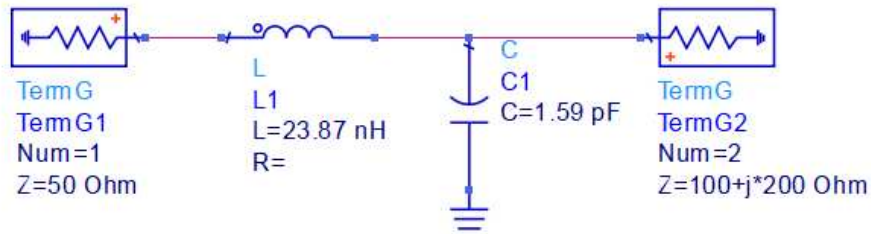
# 3 Impedance Matching Example using Calculation and Smith Chart



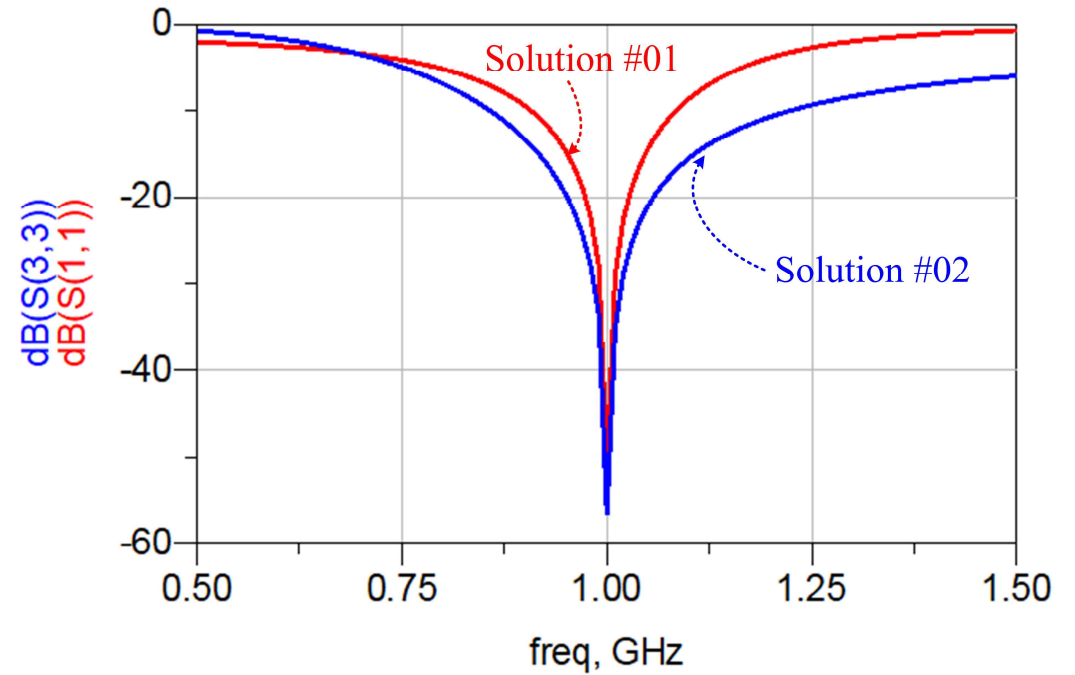
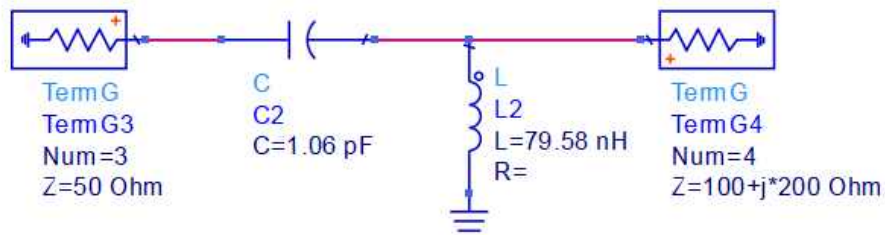
# 3

## Impedance Matching Example using Calculation and Smith Chart

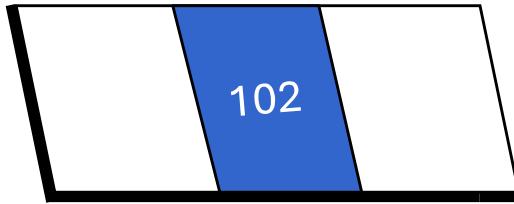
- Solution #01



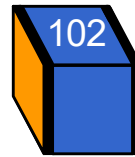
- Solution #02



## 4 Microwave Lumped Elements



planar resistor



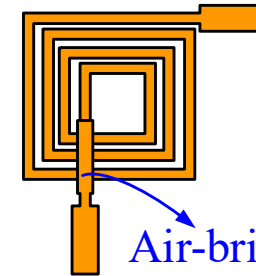
chip resistor



loop inductor

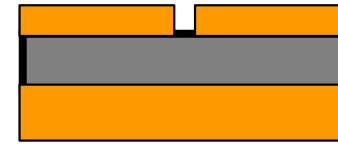
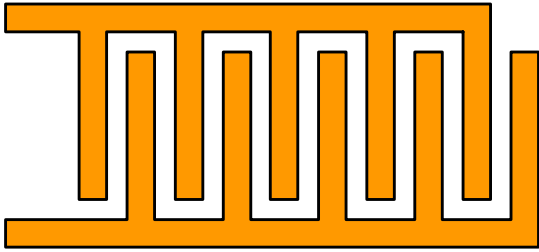


(high impedance)  
meander line inductor

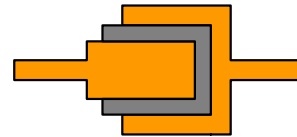
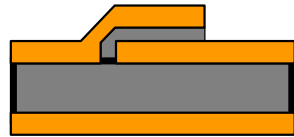
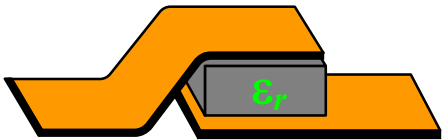


spiral inductors

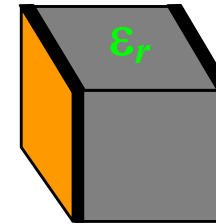
## 4 Microwave Lumped Elements



interdigital gap capacitors



Metal-insulator-metal capacitors

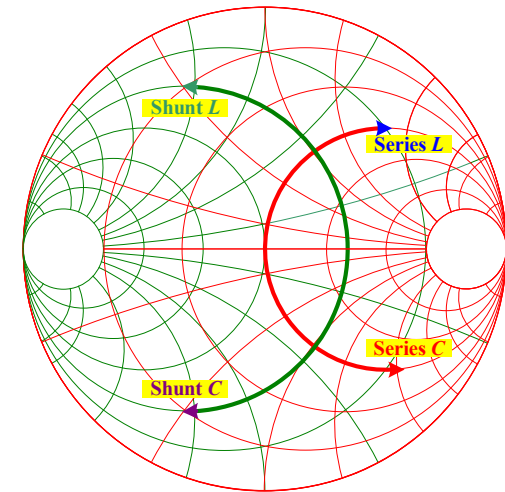
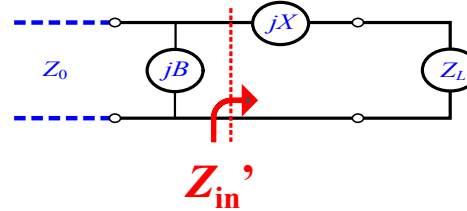
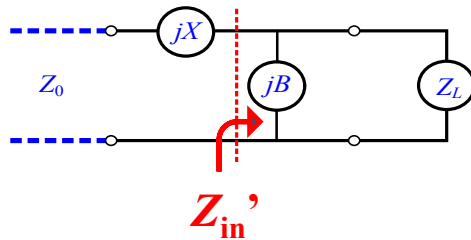


chip capacitor



## 5 Review

- Matching network useful for maximum power transmission, improvement of signal-to-noise ratio(SNR), reduction of amplitude and phase errors spatially, etc.
- L-section matching network: simplest matching network including two reactive elements



- Microwave Lumped Elements