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 $SnO_2$  quantum dots decorated on RGO: a superior sensitive, selective and reproducible performance for a  $H_2$  and LPG sensor<sup>†</sup>

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We report the H<sub>2</sub> and LPG gas sensing behavior of RGO/SnO<sub>2</sub> QDs synthesized by a surfactant assisted hydrothermal method. The RGO/SnO<sub>2</sub> QD based sensor shows a high response of ~89.3% to H<sub>2</sub> and ~92.4% to LPG for 500 ppm test gas concentration at operating temperatures of 200 °C and 250 °C, respectively. Further, the RGO/SnO<sub>2</sub> QD based sensor shows good selectivity for H<sub>2</sub> and LPG in the presence of other interfering gases such as ammonia, chloroform, toluene, benzene, acetone, *n*-butylacetate, acetic acid and formic acid. We observed that the gas response to H<sub>2</sub> is 29.8 times higher than that to acetic acid whereas the gas response to LPG is 17.8 times higher than that to formic acid. Long-term analyses have also been performed to demonstrate the reproducible nature of the RGO/SnO<sub>2</sub> QD based sensor over passing time which shows excellent reproducibility.

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### Introduction

Solid state gas sensors are well known for their high sensitivity, good selectivity and stability, which in combination with their inexpensive production, simple nature, power efficiency and miniature sizes have made them ubiquitous and extensively used in various applications.<sup>1–4</sup> Recently, a new generation of gas sensors has been reported using graphene and graphene/ metal oxide nanocomposites.<sup>5–9</sup> Among metal oxide semiconductors (MOS), tin oxide (SnO<sub>2</sub>) is particularly important, as an intrinsic n-type wide band gap (3.6 eV at 300 K) semiconductor<sup>10</sup> and has drawn much attention because of its good optical and electrical properties. It exhibits n-type conductivity due to its interstitial Sn atoms and oxygen vacancies, which

act as donors in the host matrix.<sup>11</sup> SnO<sub>2</sub> nanostructures have shown potential applications in various devices *e.g.* field effect transistors,<sup>12</sup> light emitting diodes,<sup>13</sup> dye-sensitized solar cells,<sup>14</sup> supercapacitors,<sup>15</sup> lithium ion batteries<sup>16</sup> and gas sensors.<sup>17</sup>

Graphene, a two dimensional counterpart of three-dimensional graphite, comprises a single layer of carbon atoms and is a rising star on the horizon of nano-materials & technology, solid-state physics, materials science, and nanoelectronic devices.<sup>18</sup> In addition, graphene possesses outstanding physical properties such as quantum electronic transport, extremely high mobility and high surface to volume ratio. Graphene based nanostructure materials have attracted great interest from researchers due to their numerous applications in organic light emitting diodes, solar cells, chemical and biological gas sensors,<sup>19</sup> transistors, photovoltaics, and photosensors. The commonly used methods for the preparation of graphene and reduced graphene oxide (RGO) are micromechanical cleavage of graphite,<sup>20</sup> chemical vapor deposition (CVD),<sup>21</sup> epitaxial growth,<sup>22</sup> using organic precursors,<sup>23</sup> chemical reduction of exfoliated graphene oxide<sup>24</sup> and electrochemical reduction.<sup>25</sup> Since graphene possesses a monoatomic layer structure and excellent electrical properties, it could be a fascinating material for gas sensing application. In principle, charge carriers in an individual graphene sheet delocalize over the entire sheet and can travel thousands of interatomic distances without scattering because of its zero band gap semiconducting nature, very high in-plane conductivities and very high Fermi velocity.<sup>26</sup> However, its poor interactions with



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the gas molecules and restricted diffusion in the boundaries result in low sensitivity and poor selectivity for target gases. To resolve this critical problem, different types of MOS/RGO based nanocomposites have been developed. Decoration of RGO with metal oxide nanocrystals promotes charge transfer between specific gas species, which has proven to be an effective way to improve the sensitivity, and achieve faster response/recovery and better selectivity for the specific gas at a particular operating temperature.

Hydrogen (H<sub>2</sub>) is an invisible, odorless and flammable gas for which safety becomes a primary concern, since the presence of H<sub>2</sub> concentration in excess of 4 vol% in the environment is potentially explosive.<sup>27</sup> On the other hand, liquefied petroleum gas (LPG), mainly a mixture of propane and butane is a highly inflammable gas which is regularly used in automobiles and industry and for other domestic purposes.<sup>28</sup> LPG is most commonly used in the kitchen as cooking fuel but bears high possibility of explosion accidents due to leakage/ human error or bursting of LPG filled cylinders. A small leakage may be more dangerous for living bodies as well as domestic and industrial properties. Hence, it is very important to monitor these gases in the environment and working places at its early stages to raise alarm and perform effective suppression.

Numerous efforts have been made towards the development of different types of gas sensors using nanostructure materials. Liu et al. studied a flexible, rapid-response gas sensor based on colloidal quantum dot solids.<sup>29</sup> They have demonstrated a high performance, paper-based flexible NO<sub>2</sub> gas sensor using PbS CQDs. Xu et al. reported the fabrication of a SnO2-RGO monolayer-ordered porous film gas sensor with tunable sensitivity through ultra-violet light irradiation.30 Nemade et al. synthesized graphene/SnO2 QDs through an in situ synthesis method and investigated chemiresistive gas sensing.<sup>31</sup> Invawilert et al. studied a rapid ethanol sensor based on electrolytically-exfoliated graphene loaded with a flame-made In-doped SnO<sub>2</sub> composite film.<sup>32</sup> These authors have investigated that the graphene (5 wt%) when composed with 0.5 wt% In-doped SnO<sub>2</sub> led to a drastic enhancement of response (965) along with a very short response time (1.8 s) and fast recovery stabilization at an optimal operating temperature of 350 °C. Lee et al. reported a novel approach to enhance the gas sensing properties of n-type nanofibers that involves the formation of p-n hetero-junctions with p-type RGO nanosheets.<sup>33</sup> Li et al. have developed a 3D-SnO<sub>2</sub>/RGO nanocomposite as a high performance NO<sub>2</sub> gas sensor at low operating temperatures.<sup>34</sup> The CO gas sensing properties of the direct-patternable SnO<sub>2</sub> thin films containing graphene or Ag nanoparticles have been studied by H. Kim et al.<sup>35</sup> Singkammo et al. investigated graphene loaded with a flame-made Ni-doped SnO<sub>2</sub> composite film for acetone sensing.<sup>36</sup> Recently, Liu et al. studied the chemiresistive gas sensors employing solution-processed metal oxide quantum dot films.<sup>37</sup> They have studied the detection limit of the gas sensor and observed that it was down to 6 ppb.

Herein, we studied the possibilities to detect  $H_2$  and LPG by the RGO/SnO<sub>2</sub> QD based sensing element synthesized by an *in situ* assisted hydrothermal method. Further, we have investigated the synergetic effect of RGO and  $\text{SnO}_2$  QDs on the sensing properties of H<sub>2</sub> and LPG. Here, the amount of RGO (1.0 mg in the present study) plays a vital role in improving the sensing characteristics as a combination of higher sensor response magnitude, good selectivity, excellent sensor reproducibility and short response/recovery time. The decoration of nano-sized SnO<sub>2</sub> QDs on the RGO surface was selected for this study for several reasons such as zero dimensions, high surface to volume ratio, low operating temperature and low test gas concentrations compared to other conventional sensors. High response, good selectivity and excellent reproducibility of this sensor as well as faster response and recovery to H<sub>2</sub> and LPG exposure can have a significant importance in the domestic and industrial applications.

### **Experimental details**

Graphite was purchased from Alfa Aesar whereas glucose was obtained from Merck and used without further purification. Unless otherwise stated, other reagents were of analytical grade and used as received. All aqueous solutions were prepared with ultrapure water (>18 M $\Omega$ ) from a Milli-Q Plus system (Millipore).

RGO was synthesized from graphite powder following the modified Hummers method.<sup>24</sup> The RGO/SnO<sub>2</sub> QDs were prepared by the hydrothermal method. In this process firstly, 10 mmol of SnCl<sub>4</sub>·5H<sub>2</sub>O was dissolved in distilled water to form a transparent colorless solution and then 1.0 mg RGO was added to the above solution. Subsequently, with mild stirring, 1 ml hexamethyldisilazane (HMDS) surfactant was added to the above solution. Next, the pH was maintained at 8.5 by adding a NaOH solution dropwise into the above solution. The whole solution was transferred into a 100 ml Teflon-lined stainless steel autoclave to react at 120 °C for 20 h and then allowed to cool naturally to room temperature. The obtained precipitate was separated by centrifuging at 4000 rpm for 30 minutes and washed with distilled water and ethanol several times to remove impurity ions and dried at 60 °C for 3 hours in a hot air oven. The precipitate was then calcined at 400 °C for 1 hour to obtain the final products of RGO/SnO<sub>2</sub> nanocomposites. The same experimental process was performed to prepare pure SnO2 QDs. The dried mass was then crushed into fine powder for further characterization. The fine powder of RGO/SnO2 QD nanocomposites, RGO and SnO2 QDs were pressed into pellets of 10.5 mm diameter and 1.0 mm thickness at a pressure of ~15 MPa using a hydraulic press. These pellets were further sintered at 150 °C for 30 minutes. After that, high-temperature silver paste was used for making the ohmic contacts on both surfaces of the pellet.

The shape and size of the as-prepared RGO/SnO<sub>2</sub> QDs were investigated by high resolution transmission electron microscopy (HR-TEM) on a Philips model Tecnai-20 using an accelerating voltage of 200 kV. Raman spectroscopy was performed using the Lab RAM HR 800 Microlaser Raman system in backscattering geometry using the 514.5 nm line of an Ar<sup>+</sup>-laser as an excitation source. The detailed characterization of RGO/SnO<sub>2</sub> QD, RGO and SnO<sub>2</sub> QD samples with gas sensing properties is performed and presented in the ESI.† In the present study, the H<sub>2</sub> and LPG sensor responses of RGO/SnO<sub>2</sub> QDs have been calculated using the following equation.<sup>28</sup>

$$S(\%) = \frac{R_{\rm a} - R_{\rm g}}{R_{\rm a}} \times 100 \tag{1}$$

where  $R_{\rm g}$  is the resistance of the sensor device (pellet) in the presence of gas and  $R_{\rm a}$  is the background resistance in the presence of air.

### **Results and discussion**

#### Structural studies

XRD spectra of RGO/SnO<sub>2</sub> QDs and SnO<sub>2</sub> QDs depict the tetragonal crystal structure of SnO<sub>2</sub> QDs with (110), (101), (211) and (112) diffraction planes which is consistent with JCPDS card no. 72-1147 [Fig. S1(a and c)†] whereas a broad peak observed at  $2\theta = 24.2775^{\circ}$  (*d*-spacing = 0.37 nm) is attributed to the (002) plane of RGO [Fig. S1(a and b)†]. The elemental analysis of the RGO/SnO<sub>2</sub>, RGO and SnO<sub>2</sub> QDs has been performed by XPS [Fig S2(a-c)†]. TEM, HR-TEM and selected area electron diffraction pattern (SAED) micrographs of RGO/SnO<sub>2</sub> QDs are presented in Fig. 1(a-d), to explore the structure, defects and lattice fringes. TEM images [Fig. 1(a and b)] undoubtedly indicated that the dark spots on the surface of RGO are composed of SnO<sub>2</sub> QDs. The SnO<sub>2</sub> QDs decorated on the RGO surface have also prevented the RGO from re-stacking into a multilayer.<sup>38,39</sup> The size of the  $SnO_2$  QDs is ~6 nm and shows good distribution over the RGO [Fig. 1(a and b)].

The HR-TEM image [Fig. 1(c)] shows the lattice spacing and the corresponding planes of RGO/SnO2 QDs. The lattice spacing of RGO is observed to be 0.37 nm corresponding to the (002) plane whereas  $SnO_2$  QDs have a *d*-spacing of 0.32 nm corresponding to the (110) plane. In Fig. 1(d), the SAED pattern reveals well-defined circular rings, suggesting the polycrystalline nature of the as synthesized RGO/SnO<sub>2</sub> QDs. These rings could be indexed to the (110), (101), (200), (211) & (112) planes of the SnO<sub>2</sub> phase whereas the dotted ring corresponds to the (200) plane of RGO.<sup>40,41</sup> The above result clearly suggests good polycrystallinity of RGO/SnO2 QDs. It can also be seen that each SnO<sub>2</sub> OD is attached to several other quantum dots and well dispersed on the surface of RGO [Fig. 1(a and b)]. Thus, good contact between the SnO<sub>2</sub> QDs and RGO can effectively minimize the electrical isolation of the nanostructure during the gas sensing test. RGO with higher surface area loaded with SnO<sub>2</sub> QDs can offer an improved conducting network that could facilitate electron transfer during the chemisorption process of the gas sensing. The TEM and HRTEM images of bare RGO and SnO2 QD samples are also investigated and shown in Fig. S3(a and b).† The FE-SEM and the corresponding elemental mapping images are presented in Fig. S4(a-c).<sup>†</sup> The UV-Vis studies have been performed to investigate the quantum dot nature of RGO/SnO2 QD and SnO2 QD samples [Fig. S5(a and b)<sup>†</sup>].

Raman spectroscopy is a powerful technique to characterize the RGO based material, particularly the order/disorder and defect characteristics. Fig. 2 shows Raman spectra of the as-prepared RGO/SnO<sub>2</sub> QDs. The characteristic Raman bands of RGO are observed at ~1353 cm<sup>-1</sup> (*k*-point phonons of  $A_{1g}$ symmetry, D band) and ~1579 cm<sup>-1</sup> ( $E_{2g}$  phonons of sp<sup>2</sup> atoms, G band). The G band (~1579 cm<sup>-1</sup>) is related to the



Fig. 1 (a and b) TEM, (c) HR-TEM and (d) SAED images of  ${\rm RGO}/{\rm SnO}_2$  QDs.



Fig. 2 Raman spectrum of RGO/SnO<sub>2</sub> QDs

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in-plane vibration of sp<sup>2</sup>-bonded carbon atoms whereas the D Raman band (~1348 cm<sup>-1</sup>) could be related to the breathing mode of the rings of sp<sup>2</sup>-hybridized carbon.<sup>42,43</sup> The D band indicates the presence of defect in RGO/SnO<sub>2</sub> QDs which may be associated with vacancies, grain boundaries, amorphous carbon species and disorder in the hexagonal graphitic layer.<sup>44</sup>

The Raman spectrum of RGO/SnO<sub>2</sub> QDs shows an intense G band whereas a D band of very low intensity, indicating low degree of defect in RGO. Therefore, we can say that some of these defect states arising due to nucleation centers, *i.e.* where the growth is initiated, reflects an elastic intervalley scattering process.<sup>45</sup> The existence of both G and D bands confirms the presence of RGO in the composite. The negligible intensity ratio of  $I_D/I_G$  suggests that the C=C bonds at the RGO surface are damaged in the hydrothermal synthesis process, followed by adsorption of SnO<sub>2</sub> QDs on the surface of RGO which reduced the number of oxygen-containing functional groups.<sup>40</sup>

### Gas sensing studies

#### H<sub>2</sub> and LPG sensing study

The H<sub>2</sub> and LPG gas sensing experiments were performed at different operating temperatures (150–275 °C) in order to examine the most favorable working temperature for H<sub>2</sub> and LPG gas recognition. All the gas sensing experiments were carried out at a relative humidity of ~43% under atmospheric pressure.

To avoid the interference of humidity with the sensor performance, at each particular operating temperature, the sensing element was allowed to equilibrate inside the static test gas chamber for 30 minutes before exposing to the H<sub>2</sub> and LPG gas. The H<sub>2</sub> and LPG gas sensing and the presence in different interfering vapor schematic test chambers were reported elsewhere.<sup>10,28</sup> A number of experiments have been carried out to investigate the test gas responses for various concentrations (100-500 ppm) as a function of operating temperature. The gas sensing properties of the RGO/SnO<sub>2</sub> QD based sensor strongly depends on the temperature as well as the test gas concentration. Thus the response of the RGO/SnO<sub>2</sub> QD based sensor as a function of operating temperature is mainly governed by RGO and SnO<sub>2</sub> QD surface stoichiometry and analyte-surface chemical interactions. In order to evaluate the test gas response of the RGO/SnO2 QD sensor, the change in electrical resistance was measured upon exposure to various test gas concentrations at different operating temperatures, which can be explained by a dynamic equilibrium state of adsorption and desorption.

Fig. 3(a and b) show  $H_2$  and LPG sensing response characteristics of the RGO/SnO<sub>2</sub> QDs as a function of operating temperature (150–275 °C) for various test gas concentrations (100–500 ppm), respectively. As shown in Fig. 3(a), the response increases for all  $H_2$  gas concentrations up to an operating temperature of 200 °C and found to be maximum (89.3%), after that the sensor response was observed to be



Fig. 3 Response curve of the RGO/SnO<sub>2</sub> QD based  $H_2$  (a) and LPG (b) sensor as a function of operating temperature for various test gas concentrations.

decreased. The increase in sensing response may perhaps be due to the lattice strain/structural deformation and high surface to volume ratio of SnO<sub>2</sub> QDs & RGO. Therefore, more adsorption sites are available for the adsorption of O<sub>2</sub> molecules on the surface of the RGO/SnO<sub>2</sub> QDs, resulting in higher response. It is expected that the presence of structural defects and oxygen vacancies in the RGO/SnO<sub>2</sub> QDs is more favorable for the adsorption of atmospheric oxygen on the surface of the RGO/SnO<sub>2</sub> QD sensor, leading to higher gas response. On the other hand, the response was found to be decreased with increasing temperatures beyond 200 °C. The decrease in response at higher operating temperatures is attributed to the non-availability of sufficient sensing sites on the RGO/SnO<sub>2</sub> QD surface, which may arise due to the deficiency of adsorbed atmospheric oxygen on the sensor surface. In other words, it may be due to the less interaction of the test gas with the active sites present on the sensor surface or the very poor concentration of electrons in the conduction band which interact with the atmospheric oxygen species to form active sites  $O^-$ , which is completely responsible for the gas sensing mechanism.

The changes in the gas sensing response at different operating temperatures over increased LPG concentrations have been investigated and the results are presented in Fig. 3(b). It is observed that at low operating temperatures (<200 °C) the LPG response is slow, since gas molecules do not have enough thermal energy to react with the surface adsorbed oxygen species. In fact, a potential barrier to charge transport is formed during adsorption of atmospheric oxygen on the surface or this may be due to the low diffusion or interaction of LPG molecules with RGO/SnO2 QDs at moderate temperature. However, at higher temperatures (>225 °C) the LPG response reaches its maximum response of ~92.4% at 250 °C above which the LPG response attains saturation. This may be due to the more test gas injection leading to the higher gas sensing response of the RGO/SnO<sub>2</sub> QD sensor, which might be accredited to higher surface coverage and thus more surface reaction takes place.

In other words, we can say that at an operating temperature of 150 °C, the sensing response increases for all concentrations and found to be maximum  $\sim$ 31.8% for H<sub>2</sub> [Fig. 3(a)] and ~25.6% for LPG [Fig. 3(b)] at 500 ppm concentration. This phenomenon may be attributed to the higher surface to volume ratio of the RGO supported SnO2 QDs. The gas response increases rapidly between 175 °C and 200 °C for all concentrations and reaches its maximum response of ~89.3% for 500 ppm concentration to  $H_2$  [Fig. 3(a)]. This may be due to the increased conductivity which is attributed to the thermal excitation of electrons into the conduction band of the RGO/ SnO<sub>2</sub> QDs. However, as shown in Fig. 3(b), the response to LPG is very poor in the same temperature range. Here, the LPG molecules may not have sufficient thermal energy to dissociate into its constituents to interact with active sites O<sup>-</sup> at that particular temperature, resulting in low gas response. However, at higher operating temperatures (225 °C to 275 °C), the thermal excitation of electrons and oxygen adsorption occur simultaneously<sup>46</sup> which play a vital role in both H<sub>2</sub> and LPG response. In Fig. 3(a), for all test concentrations the  $H_2$ response decreases with operating temperature. Here, the oxygen adsorption/desorption process may be dominant over the thermal excitation of electrons, therefore the response tends to decrease. But in the case of LPG, the thermal excitation of electrons may be dominant over the oxygen adsorption/desorption process resulting in higher response as shown in Fig. 3(b).47

The gas sensing results of RGO and  $SnO_2$  QDs towards  $H_2$  and LPG have also been investigated at the same operating temperature and concentration range and are presented in the ESI (Fig. S6 and Fig. S7†). It is observed that the gas sensing response of the RGO/SnO<sub>2</sub> QD based  $H_2$  and LPG sensor is superior to that of bare RGO and SnO<sub>2</sub>. This improved sensing

performance of RGO/SnO<sub>2</sub> QDs is attributed to the synergetic effect between the RGO and SnO<sub>2</sub> QDs.

Thus, the optimum working temperature for the RGO/ $SnO_2$  QDs to recognize the 500 ppm concentration of H<sub>2</sub> and LPG is 200 °C and 250 °C, respectively, which are modest from the viewpoint of gas sensors. Hence, the optimum working temperatures of 200 °C and 250 °C have been chosen in order to study the H<sub>2</sub> and LPG sensing properties such as response, selectivity, reproducibility and response/recovery times.

#### H<sub>2</sub> and LPG sensing mechanism

The H<sub>2</sub> and LPG sensing mechanism of RGO/SnO<sub>2</sub> QDs is a surface controlled process. It is based on the changes in the electrical resistance of RGO/SnO2 QDs which is controlled by the LPG and H<sub>2</sub> species and the amount of the chemisorbed oxygen on the surface of the sensor. The adsorption of the test gases, which depends on both the type of the test gas and the sensor material, affects both the response characteristics and response/recovery times. With increasing operating temperature, atmospheric oxygen is adsorbed on the surface and grain boundaries and then it exists in various forms. The adsorption of atmospheric oxygen species on the sensor surface forms ionic species such as O<sub>2</sub><sup>-</sup> and O<sup>-</sup> which acquire electrons from the conduction band of the sensing material, and this helps in understanding the gas sensing mechanism of the RGO/SnO2 QD based H<sub>2</sub> and LPG sensor. The reaction kinetics between atmospheric oxygen and the RGO/SnO2 QD sensor surface is as follows:<sup>10</sup>

$$O_2(air) \Leftrightarrow O_2(ads)$$
 (2a)

$$O_2(ads) + e^- \Leftrightarrow O_2^-(ads)$$
 (2b)

$$O_2^-(ads) + e^- \Leftrightarrow 2O^-(ads)$$
 (2c)

Thus, the immobility of the chemisorption process results in the stabilization of the sensor surface resistance. Other internal or external factors that affect the chemisorption process give rise to electrical resistance.

On injecting the reducing  $H_2$  gas into the test chamber, the  $H_2$  molecules react with the active sites  $O^-$  which are available on the surface of the RGO/SnO<sub>2</sub> QD sensor and release electrons back into the lattice tending to decrease the sensor resistance. The  $H_2$  sensing reaction mechanism has been discussed in the earlier study.<sup>48</sup>

$$H_2 + O^-(ads) \rightarrow H_2O + e^-$$
 (3)

However, the LPG sensing mechanism is a complex process and it is believed that it proceeds through several intermediate steps which are not yet understood. The reaction mechanism of LPG with chemisorbed active site O<sup>-</sup> can be written as follows:<sup>28</sup>

$$C_n H_{2n+2} + 2O^- \rightarrow C_n H_{2n} : O + e^- + H_2O$$
 (4a)

$$C_nH_{2n}: O + O^- \rightarrow CO_2 + H_2O + e^-$$
 (4b)

where  $C_nH_{2n+2}$  stands for  $CH_4$ ,  $C_3H_8$ ,  $C_4H_{10}$ , *etc.*, while  $C_nH_{2n}$ : O represents partially oxidized intermediates on the RGO/SnO<sub>2</sub> QD surface.

#### Selectivity study of H<sub>2</sub> and LPG sensor

Apart from sensitivity, selectivity is an important parameter for gas sensors. The gas responses towards a specific test gas for the same concentration are required to be noticeably higher than those to other interfering gases for selective gas detection. In the present study, the interfering gases such as ammonia, chloroform, toluene, benzene, acetone, *n*-butyl-acetate, acetic acid and formic acid have been used to study the selective behavior of the RGO/SnO<sub>2</sub> QD based H<sub>2</sub> and LPG sensor. Fig. 4(a and b) show the selective responses of the RGO/SnO<sub>2</sub> QD based H<sub>2</sub> and LPG sensor towards different interfering gases for fixed 500 ppm concentration at operating temperatures of 200 °C and 250 °C, respectively. The RGO/SnO<sub>2</sub> QD based sensor exhibits selectively higher response for 500 ppm concentration to H<sub>2</sub> (~89.3%) at an operating temperature of 200 °C whereas it shows a significantly lower



Fig. 4 Bar chart shows selective response of the RGO/SnO<sub>2</sub> QD based sensor. The gas concentration and operating temperature in all cases were 500 ppm and 200 °C for H<sub>2</sub> (a) whereas 250 °C for LPG (b) selective gas detection, respectively.

response (~3%) to acetic acid, ammonia, chloroform, toluene, benzene, *n*-butylacetate, acetone and formic acid as shown in Fig. 4(a).

On the other hand, the RGO/SnO<sub>2</sub> QD sensor also exhibits high selective performance for 500 ppm concentration to LPG (~92.4%) at an operating temperature of 250 °C compared to a very low response (5.2%) to formic acid, chloroform, ammonia, toluene, benzene, acetone, *n*-butylacetate and acetic acid as presented in Fig. 4(b). The highest response of the RGO/SnO<sub>2</sub> QD based sensor towards H<sub>2</sub> and LPG has been observed at optimum working temperatures 200 °C and 250 °C, respectively, and nearly no response to the interfering gases [Fig. 4(a and b)]. This phenomenon can be explained on the basis of the change of the resistance of the sensor caused by the charge transfer between RGO/SnO<sub>2</sub> QDs and target molecules that exhibit very good H<sub>2</sub> and LPG gas diffusivity and also good interaction with RGO and SnO<sub>2</sub> QDs rather than other interfering gases.

In order to quantify the selectivity for  $H_2$  and LPG, the selectivity coefficient ( $K_{sc}$ ) of  $H_2$  and LPG for other interfering gases has been calculated using the following equation:<sup>49</sup>

$$K_{\rm sc} = \frac{S_{\rm H_2, LPG}}{S_{\rm gas}} \tag{5}$$

where  $S_{H_2, LPG}$  and  $S_{gas}$  are the responses of the sensor to  $H_2$  & LPG and other interfering target gases, respectively, as listed in Table 1.

The selectivity coefficient " $K_{sc}$ " for the RGO/SnO<sub>2</sub> QD based H<sub>2</sub> sensor operated at 200 °C for 500 ppm concentration is the highest for acetic acid (29.8) whereas for the RGO/SnO<sub>2</sub> QD nanocomposite based LPG sensor operated at 250 °C for the same concentration it was found to be maximum for formic acid (17.8). The higher values of  $K_{\rm sc}$  show the more selective detection to H<sub>2</sub> and LPG for 500 ppm concentration at optimum working temperatures of 200 °C and 250 °C, respectively. For example, the value of  $K_{\rm sc}$  = 29.8 for acetic acid suggests that the gas response to  $H_2$  is 29.8 times higher than that to acetic acid whereas  $K_{sc}$  = 17.8 for formic acid reveals that the gas response to LPG is 17.8 times higher than that to formic acid. Thus our experimental findings indicate that the RGO/SnO<sub>2</sub> QD based sensor has a good selectivity for H<sub>2</sub> and LPG for 500 ppm concentration at optimum working temperatures of 200 °C and 250 °C, respectively. Based on the experimental observations, it can be concluded that the formation of SnO<sub>2</sub> QDs on RGO is not only effective to improve the H<sub>2</sub> and LPG responses but also makes it efficient for detection of H<sub>2</sub> and LPG.

#### Long-term reproducibility study of H2 and LPG sensor

In practical applications, besides sensitivity and selectivity, long-term reproducibility of the gas sensor is also critical for which we must determine the consistency of the gas sensor over its period of service. To justify the reproducible nature with which the RGO/SnO<sub>2</sub> QD sensor shows maximum response, the gas response measurements were tested at optimum

**Table 1** The selectivity coefficient " $K_{sc}$ " of the RGO/SnO<sub>2</sub> QD based H<sub>2</sub> and LPG sensor for different interfering gases for 500 ppm concentration at optimum working temperatures of 200 °C and 250 °C, respectively

| Interfering gases with concentration of 500 ppm |                                       |   |   |   |  |  |   |
|---|---------------------------------------|---|---|---|--|--|---|
| Ammonia   | Chloroform                            | Toluene   | Benzene   | Acetone   | N-Butylacetate   | Acetic acid  | Formic acid   |
| 12.2<br>7.9                                     | 10.6<br>5.8                           | 16.5<br>8.8   | 13.9<br>11.0  | 7.9<br>9.1  | 20.8<br>12.2   | 29.8<br>13.8   | 24.1<br>17.8  |
|   | Interfering<br>Ammonia<br>12.2<br>7.9 | Interfering gases with corAmmoniaChloroform12.210.67.95.8 | Interfering gases with concentrationAmmoniaChloroformToluene12.210.616.57.95.88.8 | Interfering gases with concentration of 500 pprAmmoniaChloroformTolueneBenzene12.210.616.513.97.95.88.811.0 | Interfering gases with concentration of 500 ppmAmmoniaChloroformTolueneBenzeneAcetone12.210.616.513.97.97.95.88.811.09.1 | Interfering gases with concentration of 500 ppmAmmoniaChloroformTolueneBenzeneAcetoneN-Butylacetate12.210.616.513.97.920.87.95.88.811.09.112.2 | Interfering gases with concentration of 500 ppmAmmoniaChloroformTolueneBenzeneAcetoneN-ButylacetateAcetic acid12.210.616.513.97.920.829.87.95.88.811.09.112.213.8 |

working temperatures of 200 °C and 250 °C for 500 ppm concentration to the  $H_2$  and LPG, respectively.

From the initial day to 50 days later, the response changed slightly by -4% to H<sub>2</sub> and -3% to LPG, demonstrating good reproducibility of the sensor as shown in Fig. 5(a and b). It has also been observed that the gas response increases sharply with insertion of H<sub>2</sub> and LPG and returns to its original state when the test gas is left out. This behavior is attributed to good electrical properties and high surface area of RGO/



Fig. 5 Long term reproducible nature of the RGO/SnO<sub>2</sub> QD sensor at operating temperatures 200 °C and 250 °C for 500 ppm concentration to the  $H_2$  (a) and LPG (b), respectively.

SnO<sub>2</sub> QDs, to interact with test gas. In addition, the rate of adsorption–desorption increases at that working temperature due to the increased diffusivity of gases at high temperatures, leading to a large number of depleted grains. Our findings conclude that RGO supported SnO<sub>2</sub> QDs have excellent reproducibility. However, the reproducibility mechanism is more complicated, and further analyses are required to gain a good understanding.

#### Real-time analyses of H<sub>2</sub> and LPG sensor

The response/recovery real-time study is an important characteristic for evaluating the performance of gas sensors. The response time is typically defined as the time taken by a sensor to read a certain percentage of full-scale reading (normally 90%) when exposed to a test gas. Similarly, the recovery time is the time taken by the sensor to return to its original state when the test gas is removed.

Fig. 6(a and b) show the response/recovery real time plot of the RGO/SnO<sub>2</sub> QDs to H<sub>2</sub> and LPG in the concentration range of 100–500 ppm at operating temperatures of 200 °C and 250 °C, respectively. It has been observed that with increasing test gas concentrations, the response time decreases which is due to increased surface coverage of the test gas molecules, resulting in the quick reaction of H<sub>2</sub> and LPG molecules with adsorbed atmospheric oxygen species. At lower test gas concentrations, the response times are more compared to recovery times because the sensor surface is insufficiently covered with the test gas molecules and therefore the reaction slows down.

It has also been noticed that LPG has low response recovery times compared to  $H_2$  except at 500 ppm concentration. This may be due to the sufficient thermal energy to excite the electrons from the valence band to the conduction band which provides more sensing sites at 250 °C compared to 200 °C. Here, it has also been observed that the gas sensing response time decreases with increasing  $H_2$  concentration [Fig. 6(a)] whereas in the case of LPG [Fig. 6(b)] the response time first increases and then decreases. It may be due to the more complex sensing mechanism of LPG which dissociates into its constituents through several intermediate steps compared to  $H_2$ , as presented in eqn (4a), (4b) and (3), respectively. In other words, we can say that the sensor temperature also regulates the activation energies of the adsorption-desorption and thereby the kinetics of surface chemisorption reaction, which is reflected in the response and recovery times of the sensor signal.



Fig. 6 The response/recovery real time plot of the RGO/SnO<sub>2</sub> QD sensor to H<sub>2</sub> (a) and LPG (b) in the concentration range 100–500 ppm at operating temperatures of 200 °C and 250 °C, respectively.

Specifically, the presence of the  $SnO_2$  QDs on the surface or into the lattice structure of RGO promotes the formation of a potential barrier between the interfaces of the two materials, which governs the electron transport properties of the nanomaterials. It may be caused by the difference in the work function of the different materials. Therefore, response and recovery times are affected correspondingly.

Thus, our experimental results of gas sensing properties reveal that the RGO/SnO<sub>2</sub> QDs have good  $H_2$  and LPG sensing properties such as higher gas response, good selectivity, short response/recovery times and excellent reproducibility at lower operating temperatures.

## Conclusions

In conclusion, the  $SnO_2$  QDs decorated on RGO have been successfully synthesized by the hydrothermal method. Structural, morphological, elemental, optical and defect

studies of the as prepared RGO/SnO<sub>2</sub> QDs were carried out by XRD, XPS, HR-TEM, FE-SEM, UV-Vis spectroscopy and Raman spectroscopy techniques. UV-Vis spectroscopy suggested the quantum confinement feature of the as-synthesized RGO/SnO<sub>2</sub> QDs [Fig. S5†]. The HR-TEM study revealed that SnO<sub>2</sub> QDs with a size less than 6 nm were anchored on the surface of RGO. The RGO/SnO<sub>2</sub> QD based sensor is demonstrated for H<sub>2</sub> and LPG gas detection for 500 ppm concentration at optimum working temperatures of 200 °C and 250 °C, respectively. Its high and fast response/recovery times as well as good sensitivity, selectivity and reproducibility make it a potential candidate for high performance H<sub>2</sub> and LPG sensors.

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