

ISSN 2287-4348

Vol. 8 No. 1



**Smart Media**  
KOREAN INSTITUTE OF SMART MEDIA  
한국스마트미디어학회



**사단법인한국전자거래학회**  
Society for e-Business Studies

# 2019 춘계학술대회

SPRING CONFERENCE OF KISM & SEBS 2019

**PROCEEDINGS**

일시 : 2019년 04월 26일(금) ~ 27일(토)

장소 : 한국교통대학교 충주캠퍼스

## 논문 발표순서 / Oral Session 1~4

### Oral Session 2 : Smart Information

4월 27일 (토) 09:00-10:30

발표장 : 한국교통대학교 충주캠퍼스 중앙도서관 605호 / 좌장 : 한복동(한국교통대)

007  
(p22)

제목 : 리뷰 속성 분류를 통한 감성 판별 방법

저자 : 임명진(조선대학교), 신주현(조선대학교)

008  
(p25)

제목 : High-Isolation Branch-Line Balun with Wideband Characteristics

저자 : Qi Wang(전북대학교), Phirun Kim(전북대학교),  
Junhyung Jeong(전북대학교), Yongchae Jeong(전북대학교)

009  
(p27)

제목 : Lung Nodule Segmentation in PETImages using Deep Neural Networks

저자 : Duc-Ky Ngo(전남대학교), 이귀상(전남대학교), 김수형(전남대학교),  
양형정(전남대학교)

010  
(p29)

제목 : 실시간 시선 추적기반 스마트 의료기기 고찰

저자 : 박정훈(삼성전자 AI센터), 임강빈(순천향대학교)

011  
(p33)

제목 : 지능형 영상, 음성 패턴 알고리즘 기반 Home Security 시스템

저자 : 김시원(한국교통대학교), 정주호(한국교통대학교), 오염덕(한국교통대학교),  
안준호(한국교통대학교), 이광(한국교통대학교)

012  
(p36)

제목 : 마이크로파 선형 전력증폭기를 위한 신호 조건에 따른 상쇄특성 연구

저자 : Phanam Pech(전북대학교), 정준형(전북대학교),  
Girdhari Chaudhary(전북대학교), 정용채(전북대학교)

# High-Isolation Branch-Line Balun with Wideband Characteristics

Qi Wang<sup>#</sup>, Phirun Kim<sup>#</sup>, Junhyung Jeong<sup>#</sup>, and Yongchae Jeong<sup>#1</sup>

<sup>#</sup>Division of Electronics Engineering, Chonbuk National University,

Jeonju-si, Republic of Korea

E-Mail : <sup>1</sup>ycjeong@jbnu.ac.kr

## Abstract

This paper presents a design of high-isolation branch-line balun with wideband characteristics. The high isolation can be obtained by adding a shunt coupled-line open-stub and a resistor between the output ports. The branch line balun was designed at center frequency ( $f_0$ ) of 3.5 GHz. The simulated bandwidth of 20 dB return loss is 0.91 GHz (3.05–3.96 GHz). The power divisions of 3.05 dB at  $f_0$  are obtained. The isolation better than 20 dB is obtained over a bandwidth of 1.318 GHz (2.887–4.205 GHz). The simulated phase imbalance is better than  $180 \pm 8^\circ$  over the bandwidth of 0.91 GHz.

## 1. Introduction

High-isolation branch-line balun have been researched and applied in many applications such as push-pull amplifier [1], antennas [2], and mixers [3]. In [4], a three-layer wideband Marchand balun was presented using slot-coupled microstrip lines. This work did not consider isolation characteristics between the output ports. Marchand baluns with high isolation characteristics were introduced in [5], [6]. These works were considered only at the center frequency ( $f_0$ ), which can provide a narrow bandwidth characteristic. Three-ports baluns composed of symmetrical four-ports branch-line structures by a terminating an open-circuited port were reported in [7], [8]. In [8], a branch-line balun with stubs on vertical branches, which can eliminate unwanted even-mode capacitance and reduce overall circuit size, was presented. However, the circuit performances had relatively narrow bandwidths and did not consider the isolation characteristic between output ports.

In this paper, wideband high isolation branch-line balun is proposed. The general designed equations are derived. The high isolation can be obtained by using open-circuit parallel coupled line and a shunt resistor at the output ports.

## 2. Design Equations

Fig. 1 shows the proposed structure of high-isolation wideband branch-line balun. The proposed circuit consists of a pair of horizontal quarter-wavelength ( $\lambda/4$ ) transmission lines (TLs) with characteristic impedance  $Z_2$  and a pair of vertical half wavelength ( $\lambda/2$ ) TLs with characteristic impedances  $Z_1$ . The parallel coupled lines connected back-to-back with a shunt resistor at the center of the

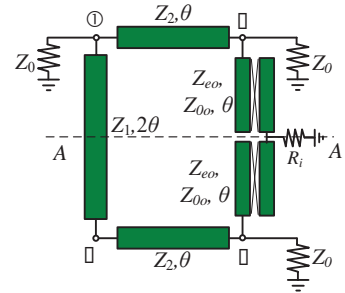


Fig. 1. Proposed high isolation wideband balun structure.

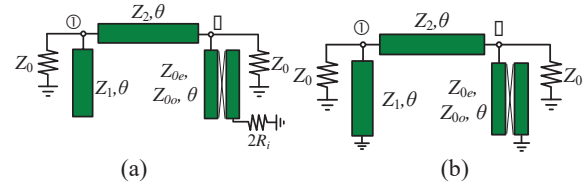


Fig. 2. Equivalent circuits: (a) even- and (b) odd-modes.

coupled line are used for the wideband high isolation characteristic. From [7], the even- and odd-mode excitations are applied to derive design equations. The even- and odd-mode equivalent circuits of proposed circuits are shown in Figs. 2(a) and 2(b), respectively. Under the even-mode excitation, the symmetrical plane of AA' can be considered as a perfect magnetic wall (open-circuited). Under the odd-mode excitation, the symmetrical plane of AA' can be considered as a perfect electric wall (short-circuited). From Fig. 2(b), the  $S_{11}$  at  $f_0$  of the odd-mode equivalent circuit can be derived as (1).

$$S_{11}|_{f=f_0} = \frac{Z_2^2 - 2Z_0^2}{Z_2^2 + 2Z_0^2} \quad (1)$$

From (1), the characteristic impedance of  $Z_2$  with the

specific  $S_{11}$  at  $f_0$  can be found as (2).

$$Z_2 = Z_0 \frac{2(1 - S_{11}|_{f=f_0})}{1 + S_{11}|_{f=f_0}} \quad (2)$$

The even-mode impedance ( $Z_{0e}$ ) of the coupled line can be found as (3) by setting  $S_{11} = 0$ .

$$Z_{0e} = \frac{(2Z_{0o} + p) + \sqrt{p(8Z_{0o} + p)}}{2}, \quad (3a)$$

where

$$p = \frac{2Z_1 Z_2}{2(Z_1 + Z_2) - Z_1}. \quad (3b)$$

$Z_1$  and  $Z_{0o}$  can be chosen arbitrarily and  $Z_2$  can be found from (2).

From Fig. 2(a), the isolation resistor  $R_i$  is split in half along the axis-AA'. The resistance  $R_i$  can be found as (4) with the specific isolation  $S_{23}|_{f_0}$ .

$$R_i = \frac{(Z_{0e} - Z_{0o})^2 \left[ 2Z_0^2 - S_{23}|_{f_0} (Z_2^2 + 2Z_0^2) \right]}{Z_L 8 \left[ S_{23}|_{f_0} (Z_2^2 + 2Z_0^2) + Z_2^2 \right]}, \quad (4)$$

where  $S_{23}|_{f_0}$  is the magnitude of the isolation at  $f_0$ .

The design procedure of proposed balun is summarized as follow. Firstly, specify  $Z_{0o}$ ,  $Z_1$ ,  $f_0$ ,  $S_{11}|_{f_0}$ , and  $S_{23}|_{f_0}$ . Then  $Z_2$ ,  $Z_{0e}$ , and  $R_i$  can be calculated from (2), (3), and (4), respectively.

### 3. Design Example

To validate the proposed circuit and designed equations, a wideband high isolation branch-line balun was designed at  $f_0 = 3.5$  GHz with 20 dB return loss and isolation at  $f_0$ . The characteristic impedances of  $Z_1 = 70 \Omega$ ,  $Z_{0o} = 55 \Omega$ , and  $S_{11}|_{f_0} = S_{23}|_{f_0} = 20$  dB were chosen. From (2), (3), and (4),  $Z_2 = 63.9602 \Omega$ ,  $Z_{0e} = 151.7051 \Omega$ , and  $R_i = 19.1288 \Omega$  are calculated, respectively. The simulation is performed using ADS tool. Fig. 4 shows the S-parameter characteristics of the proposed wideband branch-line balun. From the simulation, the return loss of 20 dB is obtained at  $f_0$ . The bandwidth of 20 dB return loss is 0.91 GHz (3.05 – 3.96 GHz).  $S_{21} = S_{31} = 3.05$  dB is obtained at  $f_0$ , respectively. The amplitude imbalance better than  $\pm 0.3$  dB is obtained within the bandwidth of 0.91 GHz. The isolation between the output ports is obtained as 20 dB at  $f_0$ . Isolation better than 20 dB is obtained over a bandwidth of 1.318 GHz (2.887– 4.205 GHz). The simulated phase imbalance between two output ports is better than  $180 \pm 8^\circ$  over the bandwidth of 0.91 GHz.

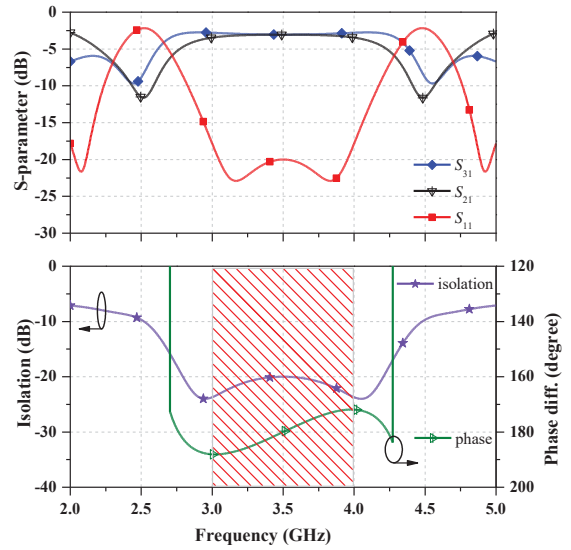


Fig. 3. Frequency response of proposed wideband balun high isolation (@ $Z_0=50 \Omega$ ).

### 4. Conclusion

In this paper, a wideband branch line balun is proposed. The high isolation can be obtained within a wideband characteristic using shunt coupled lines and a shunt resistor between the output ports. The magnitude of return loss and isolation at center frequency can be chosen arbitrarily. The low phase imbalance can be obtained over the wideband. The proposed circuit is simple to design and can be applicable for wideband RF systems.

### References

- [1] E. Serbryakova, A. Samulak, K. Blau, and M. Hein, "Reconstruction filters for switched-mode power amplifier systems," *Proceedings of 39th European Microw. Conf.*, pp. 1453–1456, 2009.
- [2] J. Jeong, I. Yom, and K. Yeom, "An active IF balun for a double balanced resistive mixer," *IEEE Microw. Wireless Compon. Lett.*, vol. 19, no. 4, pp. 224–226, Apr. 2009.
- [3] P. Nguyen, A. Abbosh, and S. Crozier, "Wideband and compact quasi-Yagi antenna integrated with balun of microstrip to slotline transitions," *Electronics Lett.*, vol. 49, no. 2, pp. 88–89, 2013.
- [4] C. Tseng and Y. Hsiao, "A new broadband marchand balun using slot-coupled microstrip lines," *IEEE Microw. Wireless Compon. Lett.*, vol. 20, no. 3, pp. 157–159, Mar. 2010.
- [5] H. Anh and S. Nam, "New design formulas for impedance-transforming 3-dB marchand balun," *IEEE Trans. Microw. Theory Techn.*, vol. 59, no. 11, pp. 2816–2823, Nov. 2011.
- [6] M. Chongcheawchamnan, C. Yong-Ng, K. Bandudej, A. Worapishet, and I. D. Robertson, "On miniaturization isolation network of an all-ports matched impedance-transforming marchand balun," *IEEE Microw. Wireless Compon. Lett.*, vol. 13, no. 7, pp. 281–283, Jul. 2003.
- [7] Y. Leong, K. Ang, and C. Lee, "A derivation of a class of 3-port baluns from symmetrical 4-port networks," *IEEE Internat. Microw. Symposium Digest*, pp. 1165–1168, 2002.
- [8] J.-L. Li, S.-W. Qu, and Q. Xue, "Miniaturised branch-line balun with bandwidth enhancement," *Electronics Lett.*, vol. 43, no. 17, pp. 931–932, 2007.