ISSN 2287-4348

ISITC 2014

2014 International Symposium on Information Technology Convergence

KISM Fall Conference 2014

2014 Korean Institute of Smart Media Fall Conference

(Vol.3 No.2)

October 30-31, 2014 Chonbuk National University, Korea http://kism.or.kr/ISITC2014



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Tunable Negative Group Delay Circuit With Improved Signal Attenuation

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Abstract

In this paper, a design of tunable negative group delay circuit (NGDC) with improved signal attenuation is presented. The proposed circuit is based on reflective parallel RLC circuit and the group delay (GD) can be tuned with help of variable capacitor. To maintain constant resonance center frequency due to capacitance variation, variable inductor is applied in the proposed NGDC. To get the variable capacitor and inductor, varactor diode and transmission line terminated with varactor diode, respectively, are used. Both design equations and design procedures are presented. The measured GD and insertion loss variation range is $-2 \sim -20$ ns and $4.45 \sim 23.2$ dB.

Keywords- negative group delay circuit, varactor diode, transmission line.

I. Introduction

Since after discovery of negative group delay (NGD) concept, it has been applied to the various applications of microwave communication system [1]-[5]. For example, by inserting negative group delay circuit (NGDC) on a common path in the feed-forward amplifier, it is possible to remove group delay (GD) circuit located in the output port of main power amplifier, which results in enhancements of overall efficiency and output power [6]. The previous NGDC can provide tunable NGD. However, main drawback of NGDCs have high insertion loss [7]. This high insertion loss is a limitation for applying NGDCs in microwave communication systems.

This paper presents the analysis and design of tunable NGDC with improved signal attenuation. For this purpose, the variable capacitor and inductor are implemented with varactor diode and transmission line (TL) terminated with the varactor diode, respectively.

II. Mathematical Analysis

Fig. 1(a) shows the structure of proposed tunable NGDC. It consists of 3-dB hybrid coupler, varactor diode, and TL terminated with the varactor diode, respectively. The equivalent circuit of coupling and through port circuits is shown in Fig. 1(b) as an 1-port parallel RLC equivalent circuit. In this equivalent circuit, the varactor is expressed along with parasitic components such as junction capacitance C_{VP} , junction resistance R_{VS} , and lead inductance L_{VP} .

At the resonant frequency, the GD and insertion loss expressions can be obtained as follows.

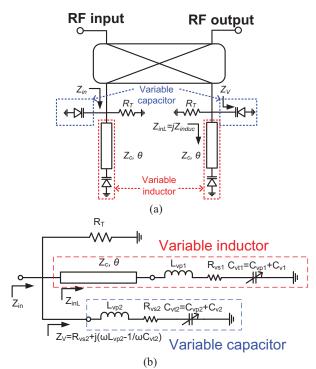


Fig. 1 (a) Proposed tunable negative group delay circuit with improved signal attenuation structure and (b) equivalent circuit of 1-port parallel RLC with varactor diodes.

$$GD\Big|_{\omega=\omega_0} = \frac{Z_0 R_T^{3} Z_V \left(Z_{induc} + \omega_0 Z_{induc}' \right)}{Z_I \left(R_T^{2} - Z_0^{2} \right)}$$
(1)

$$\left|S_{21}\right|_{\omega=\omega_{0}} = \frac{R_{T} - Z_{0}}{R_{T} + Z_{0}} \tag{2}$$

where

$$Z_{induc} = jZ_C \frac{\omega_0 C_{vt1} Z_C + \omega_0^2 C_{vt1} L_{vp1} - 1}{\omega_0 C_{vt1} Z_C - \omega_0^2 C_{vt1} L_{vp1} + 1} = \frac{1}{\omega_0 Z_V} \bigg|_{\omega = \omega_0}$$
(3)

$$Z_{induc} = Z_C \frac{-2C_{v1}Z_C \left(\omega^2 C_{v1}L_{vp1} - 1\right) + 4\omega^2 C_{v1}^2 L_{vp1}Z_C}{\left(\omega C_{v1}Z_C - \omega^2 C_{v1}L_{vp1} + 1\right)^2}$$
(4)

$$C_{\nu\nu1} = \frac{Z_C \omega_0 Z_V + 1}{\left(\omega_0^2 Z_V Z_C^2 + \omega_0^3 Z_V L_{\nu\nu1} Z_C + \omega_0^2 L_{\nu\nu1} - \omega_0 Z_C\right)}$$
(5)

From (1), NGD can be obtained for $0 < R_T < Z_0$. It is also clear that the GD can be tuned with variable R_T . Also Z_V and Z_{induc} can vary GD, respectively, but these values must have trade-off relation for maintain the constanct resonance frequency.

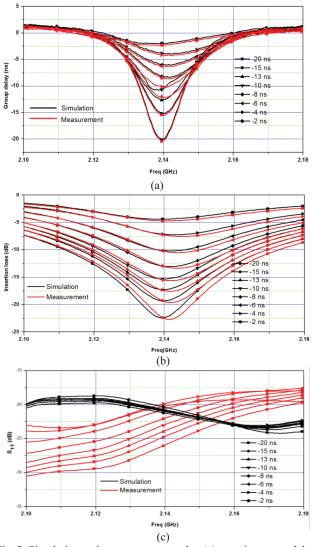


Fig. 2. Simulation and measurement results: (a) negative group delay, (b) insertion loss, and (c) return loss characteristics.

Expressions (3) and (4) are input impedance and differential value of variable inductor, respectively, where these values can be selected by (5). In (5), C_{vtl} is varacter diode capacitance of variable inductor for maintaining the constanct resonance frequency

As senn from (2), the signal attenuation characteristic is function of R_T at resonant frequency. The signal attneuation is increased when R_T is closer to Z_0 . Therefore, the NGD with improved signal attneuation can be obtained by low resistance.

III. Simulation and Measurement

For experimental validation, NGDC with GD variation of -2~-20 ns at center frequency (f_0) of 2.14 GHz for WCDMA downlink band was designed. The circuit is fabricated on the substrate RT/Duriod 5880 from Rogers Inc. with a dielectric constant (ε_r) of 2.2 and thickness (h) of 31 mils. The varacter diode SMV 1233 from Skyworks for the variable capacitor and TL with characteristic impedance of Z_c =80 Ω and electrical length of θ =45° for variable inductor were used. Parasitic components (C_{VP} , R_{VS} and L_{VP}) of varactor diode from the data sheet are 0.8 pF, 1.3 Ω , and 1.5 nH respectively.



Fig. 3. Photograph of fabricated circuit.

Fig. 2 shows the simulated and measured results of the fabricated tunable NGDC with improve signal attenuation. The measured results are well agreed with the simulation results. From Fig. 2(a), the GD variation is from -2 ns to -20 ns at f_0 . The measured insertion loss variations is shown in Fig. 2(b), where its magnitude varies from 4.45 dB to 23.2 dB. The measured return loss characteristics are higher than 17.5 dB for overall tunable range as shown in Fig. 2(c). Fig. 3 shows the photograph of fabricated circuit.

IV. Conclusion

This paper presented analysis and design of tunable negative group delay circuit with improve signal attenuation for WCDMA downlink band. The proposed circuit showed the group delay variation of -2 to -20 ns at the center frequency. For group delay of -20 ns, the insertion loss in proposed work have only 23.2 dB whereas 35 dB and 46.12 dB in [6] and [7]. Therefore, the proposed work provides an improvement in an insertion loss as compared to conventional circuits and therefore, reduce a burden of general purpose gain compensating amplifiers. The proposed circuit is expected to be applicable in various microwave communication systems.

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